by<br>Jason Weiger


#### Abstract

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#### Abstract

JASON WEIGER. Load rating for North Carolina legal vehicles. (Under the direction of DR. THOMAS NICHOLAS II)


Bridge load rating is the process by which the continued health and capacity of bridges are determined by state authorities. This process was established after the collapse of the Silver Bridge over the Ohio River due to overloading resulted in 46 deaths and has been federally mandated since 1968 . NCDOT currently uses 29 legal vehicles to load rate bridges, of which 16 are generated by NC general statutes. Most states have successfully optimized their rating vehicles to fewer than five legal vehicles for the same purpose. The work presented in this thesis provides a proposed methodology to optimize the number of legal vehicles used by NCDOT. Values were calculated for maximum bending moment, lowest operating weight, and lowest posting weight for the current legal vehicles. Steel girder bridges with spans ranging between 19.5 ft . and 162.9 ft . were tested at varying levels of effectiveness and section modulus loss. The resulting values for the vehicle operating weights of the legal vehicles were then used to determine the impact of degradation on the controlling posting vehicles. This process showed that seven of the sixteen vehicles used to load rate non-interstate bridges were redundant in the load rating process for steel girder bridges. Additionally, a computer program was developed to generate potential legal vehicles that comply with North Carolina general statutes determining maximum vehicle weights. This can be utilized by NCDOT to replace the current legal vehicle representing cotton trucks, which was found to be non-compliant with the general statute.

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"No man is an island, though too many think they can be a peninsula."

- Anonymous

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## LIST OF ABBREVIATIONS

| AASHTO | American Association of State Highway and Transportation <br> Officials |
| :--- | :--- |
| GDF | Girder Distribution Factor |
| LRFR | Load and Resistance Factor Rating |
| NBIS | National Bridge Inspection Standards |
| NCDOT | North Carolina Department of Transportation |
| RF | Rating Factor |
| STAA | Surface Transportation Assistance Act |
| SV | Single-Unit Vehicles |
| TT | Tractor Truck Semi Trailers |
| WIGINS | Wearable Inspection and Grading Information Network System |

## Chapter 1: Introduction

### 1.1 Problem Statement

The North Carolina Department of Transportation (NCDOT) is currently responsible for managing 18,169 structures. This includes 13,558 bridges, as well as 4,611 pipes and culverts with a minimum span of twenty feet and are thus classified as bridges. As of 2013, over 4000 of these structures are weight restricted (ASCE, 2013), and this number is expected to rise as inventory continues to age. The NCDOT follows the National Bridge Inspection Standards; these standards require every bridge to be inspected every two years. Any inspected bridge that no longer performs at the original design load levels is evaluated based on Legal Loads as described by North Carolina general statutes.

The NCDOT currently load rates bridges for thirteen vehicles that can legally travel on interstate highways and sixteen vehicles that can legally travel on non-interstate highways as broadly described by NC general statutes (GS §20-118). The NC general statutes provides allowable axle loads at varying spacing, grouped into single vehicles (SV) and tractor truck semi-trailers (TT). The process of determining the controlling load rating (or vehicle) is cumbersome, especially on multi-span bridges. Maintenance of the fleet of vehicles required to perform these load ratings on the 13,500 bridges managed by the NCDOT is unnecessarily burdensome. Many states have optimized their respective legal loads to a more manageable number of rating and posting vehicles, in an effort to streamline the live load generation process.

### 1.2 Objectives and Scope of Study

The objectives of this study are as follows:

1. Develop a methodology to optimize existing NC posting vehicles. Efforts included in this task will result in development of a framework to reduce the number of vehicles currently used to load rate bridges. The methodology will be based on current NCDOT bridge load rating practices as well as the use of influence lines to determine maximum moment envelopes produced by legal vehicles at varying span lengths.
2. Utilize the developed framework to optimize the list of posting vehicles. The methodology developed in task 1 will be used to define groups of vehicles that produce similar load effects on the spans and to identify specific vehicles that can represent the group.
3. Develop an automated computer program that generates NC posting vehicles from NC general statutes. The program will utilize the axle loading matrix found in NC general statute §20-118 along with user-defined parameters and will return a list of trucks sorted by maximum bending moment. The program will be written in C and will concentrate on single vehicles with 2 to 7 axles, and tandem trucks with 3 to 7 axles.

### 1.3 Organization of thesis

This thesis consists of six chapters. In the first chapter, the problem statement is presented, and the scope and objectives of the study are described. In the second chapter,
the literature review describes the current state of practice for bridge loading and presents previous work on the Muller-Breslau principle (influence lines) and the determination of live load envelopes. In the third and fourth chapters, the methodologies utilized in this study are specified: in the third chapter, optimization of the legal posting vehicles is investigated, and chapter four presents the generation of the automated computer model. The results of the methodologies are presented in the fifth chapter. The summary and conclusion of the study are provided in the sixth chapter.

## Chapter 2: Literature Review

### 2.1 Introduction

The following literature review describes the current state of practice governing the regulations of vehicle weights for both federal and state mandated vehicles. The history of federal legislation is provided, and the establishment of grandfather clauses permitting oversized vehicles is highlighted. The literature review identifies the relevant statutes in North Carolina law that govern vehicle weight limits, as well as the vehicle exceptions written into state law. A state-by-state review of load rating processes was conducted. The literature review provides a foundation of similar work to the development of equivalent uniform live load envelopes (Schaffer, 1952), where maximum moments and shears were calculated for bridges consisting of different numbers of lane and lane widths; these maximum moments and shears for each discrete bridge condition were combined to form the load envelope, a tool that identifies the range of the effects of load at all locations along a member. Load envelopes have been developed utilizing nonlinear analysis of bridges subjected to moving loads; the moment or shear failure at three critical locations were analyzed to produce the influence lines for the structure (Fiorillo, 2015).

### 2.2 Current State of Practice

Regulation of truck size and weight was first mandated by the federal government with the Federal-Aid Highway Act of 1956. In this legislation, the weight limits on trucks operating on the Interstate system were delineated to prevent the premature deterioration of the newly-created highways. Regulated vehicle weights included a maximum single axle weight of $18,000 \mathrm{lbs} .$, a maximum tandem axle weight of $32,000 \mathrm{lbs}$., and a maximum overall gross vehicle weight of $73,280 \mathrm{lbs}$. These vehicle weight limits are codified by Title 23 USC§127, Vehicle Weight Limitations, Interstate System. The 1956 Federal-Aid Highway Act also allowed states to exempt vehicles that exceeded federal weight limits, provided that the states had such vehicle weight laws in effect in 1956 (Tabsh and Tabatabi, 2001). The National Bridge Inspection Standards (NBIS) were introduced in the FederalAid Highway Act of 1968, in response to the "Silver Bridge" bridge failure in 1967. The NBIS regulations require that each bridge be rated with respect to the AASHTO Design Manual or restricted based on state law when the operating loads are exceeded. Each state has established legal live loads based on tire, wheel, single axle, tandem axles and/or gross vehicle weight meeting or exceeding federally mandated weight limits for interstate systems and safe vehicle weights for state roadway systems. Although the federal limits on axle loads were raised by the Federal-Aid Highway Amendments of 1974, these increases were not mandatory; furthermore, a provision in those amendments permitted states with existing weight tables or axle spacing formulas to be exempt from the new requirements. These increased weight limits were imposed by law in 1982 when Congress passed the Surface Transportation Assistance Act (STAA). The federal weight limits have not been altered since 1982; the current federal weight limits include a single axle maximum weight
of $20,000 \mathrm{lbs}$. , a maximum tandem axle weight of $34,000 \mathrm{lbs}$., and a maximum gross vehicle weight of $80,000 \mathrm{lbs}$. (Fox, 2015).

North Carolina had truck weight laws in effect by 1956, and those laws have been grandfathered in all subsequent laws pertaining to trucks operating on the federal national network. Single axle and gross vehicle weight maximums match federal law; however, North Carolina allows a maximum tandem axle load of $38,000 \mathrm{lbs}$., an additional $10 \%$ tolerance to state limits that does not apply to single axle, tandem axle, or gross vehicle weight limits, and numerous commodity-specific weight exceptions, as specified in North Carolina general statute §20-118 and detailed below.


Figure 2.1: Tandem truck, single/tandem axles.

## Vehicle Weight Limits

The statute specifies the following weight limits to vehicles operating on state highways:

- Single axle maximum: $20,000 \mathrm{lb}$.
- Tandem axle maximum: $38,000 \mathrm{lb}$.
- Gross weight maximum: based on the matrix found in §20-118(b)(3), as shown below in Figure 2.2.


## Exceptions

The statute exempts eight classes of vehicles from one or more of the above restrictions:

1. Garbage. This exception applies to "fully enclosed motor vehicles designed specifically for collecting, compacting and hauling garbage from residences or from garbage dumpsters."
2. Agriculture: including dairy and crop products; water, fertilizer, pesticides, seeds, fuel, or animal waste; meats, livestock, or live poultry; feeds, or feed ingredients; forest products, wood residuals, raw logs, or Christmas trees. These exceptions apply for vehicles transporting the above materials within 150 miles of point of origin.
3. Aggregates. This exception applies to vehicles hauling aggregates "from a distribution yard or State-permitted production site" to a location across a contiguous state line.
4. Mineral: including soil, rock, sand, or asphalt millings. This exception applies to vehicles transporting the above materials "from a site that does not have a certified scale for weighing the vehicle."
5. Concrete. This exception applies to vehicles "hauling unhardened readymix concrete."

| Axles* | 2 Axles | 3 Axles | 4 Axles | 5 Axles | 6 Axles | 7 Axles |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 38000 |  |  |  |  |  |
| 5 | 38000 |  |  |  |  |  |
| 6 | 38000 |  |  |  |  |  |
| 7 | 38000 |  |  |  |  |  |
| 8 or |  |  |  |  |  |  |
| less | 38000 | 38000 |  |  |  |  |
| more |  |  |  |  |  |  |
| than 8 | 38000 | 42000 |  |  |  |  |
| 9 | 39000 | 42500 |  |  |  |  |
| 10 | 40000 | 43500 |  |  |  |  |
| 11 |  | 44000 |  |  |  |  |
| 12 |  | 45000 | 50000 |  |  |  |
| 13 |  | 45500 | 50500 |  |  |  |
| 14 |  | 46500 | 51500 |  |  |  |
| 15 |  | 47000 | 52000 |  |  |  |
| 16 |  | 48000 | 52500 | 58000 |  |  |
| 17 |  | 48500 | 53500 | 58500 |  |  |
| 18 |  | 49500 | 54000 | 59000 |  |  |
| 19 |  | 50000 | 54500 | 60000 |  |  |
| 20 |  | 51000 | 55500 | 60500 | 66000 |  |
| 21 |  | 51500 | 56000 | 61000 | 66500 |  |
| 22 |  | 52500 | 56500 | 61500 | 67000 |  |
| 23 |  | 53000 | 57500 | 62500 | 68000 |  |
| 24 |  | 54000 | 58000 | 63000 | 68500 | 74000 |
| 25 |  | 54500 | 58500 | 63500 | 69000 | 74500 |
| 26 |  | 55500 | 59500 | 64000 | 69500 | 75000 |
| 27 |  | 56000 | 60000 | 65000 | 70000 | 75500 |
| 28 |  | 57000 | 60500 | 65500 | 71000 | 76500 |
| 29 |  | 57500 | 61500 | 66000 | 71500 | 77000 |
| 30 |  | 58500 | 62000 | 66500 | 72000 | 77500 |
| 31 |  | 59000 | 62500 | 67500 | 72500 | 78000 |
| 32 |  | 60000 | 63500 | 68000 | 73000 | 78500 |
| 33 |  |  | 64000 | 68500 | 74000 | 79000 |
| 34 |  |  | 64500 | 69000 | 74500 | 80000 |
| 35 |  |  | 65500 | 70000 | 75000 |  |
| 36 |  |  | $66000 * *$ | 70500 | 75500 |  |
| 37 |  |  | 66500** | 71000 | 76000 |  |
| 38 |  |  | 67500** | 72000 | 77000 |  |
| 39 |  |  | 68000 | 72500 | 77500 |  |
| 40 |  |  | 68500 | 73000 | 78000 |  |
| 41 |  |  | 69500 | 73500 | 78500 |  |
| 42 |  |  | 70000 | 74000 | 79000 |  |
| 43 |  |  | 70500 | 75000 | 80000 |  |
| 44 |  |  | 71500 | 75500 |  |  |
| 45 |  |  | 72000 | 76000 |  |  |
| 46 |  |  | 72500 | 76500 |  |  |
| 47 |  |  | 73500 | 77500 |  |  |
| 48 |  |  | 74000 | 78000 |  |  |
| 49 |  |  | 74500 | 78500 |  |  |
| 50 |  |  | 75500 | 79000 |  |  |
| 51 |  |  | 76000 | 80000 |  |  |
| 52 |  |  | 76500 |  |  |  |
| 53 |  |  | 77500 |  |  |  |
| 54 |  |  | 78000 |  |  |  |
| 55 |  |  | 78500 |  |  |  |
| 56 |  |  | 79500 |  |  |  |
| 57 |  |  | 80000 |  |  |  |

Figure 2.2: Vehicle gross weight limits, according to NC general statute §20-118(b)(3).
6. Utility: including vehicles owned by, operated by, or under contract to a "public utility, electric or telephone membership cooperation."
7. Construction: including vehicles hauling construction equipment or metal commodities.
8. Cotton. This exception applies to vehicles "equipped with a self-loading bed ... which is designed and used exclusively to transport compressed seed cotton from the farm to a cotton gin, or sage to market.

The exceptions placed in the statute for the vehicles listed above are as follows:

- Garbage: steering axle maximum $=23,500 \mathrm{lbs}$.
- Agriculture: An agriculture vehicle is excepted if it meets any of the three configurations:
- Single axle maximum $=22,000$ lbs.; tandem axle maximum $=$ $42,000 \mathrm{lbs} . ;$ gross weight maximum $=90,000 \mathrm{lbs}$.
- Five (or more) axles; minimum wheelbase $=48$ feet; single axle maximum $=26,000 \mathrm{lbs} . ;$ tandem axle maximum $=44,000 \mathrm{lbs} . ;$ gross weight maximum $=90,000 \mathrm{lbs}$.
- Two axles; minimum wheelbase $=14$ feet; Single axle maximum = 27,000 lbs.; gross weight maximum $=37,000 \mathrm{lbs}$.
- Aggregates: gross weight maximum $=69,500 \mathrm{lbs} . ;$ tri-axle maximum $=$ 53,580 lbs.
- Mineral: Single axle maximum $=22,000 \mathrm{lbs} . ;$ tandem axle maximum $=$ $42,000 \mathrm{lbs} . ;$ gross weight maximum $=4,000 \mathrm{lbs}$. in excess of gross weight maximum found in §20-118(b)(3).
- Concrete: A concrete vehicle is excepted if it meets all of the following conditions:
- Single axle maximum $=22,000$ lbs.; tandem axle maximum $=$ 46,000 lbs.
- Three axle vehicle with a minimum wheelbase of 21 feet: gross weight maximum $=66,000 \mathrm{lbs}$.
- Four axle vehicle with a minimum wheelbase of 36 feet: gross weight maximum $=72,600 \mathrm{lbs}$.
- Utility: single axle maximum $=28,000$ lbs.; gross weight maximum $=$ 48,000 lbs.
- Construction: single axle maximum $=26,000 \mathrm{lbs}$.; tandem axle maximum = $44,000 \mathrm{lbs}$.; gross weight maximum $=90,000 \mathrm{lbs}$.
- Cotton: tandem axle maximum $=50,000 \mathrm{lbs}$.

The possible load combinations derived from these matrices can be cumbersome to the bridge rating engineer in determining live load envelops. In an effort to streamline the live load generation process some states have optimized their respective legal loads to a more manageable number of rating/posting vehicles. A state-by-state review of load rating processes was performed, and the results are summarized in Table 1. Three states do not make their load rating process publicly available. One state does not include vehicle or legal load data in their publicly-available literature. Twenty-six states specify legal vehicles
in their load rating processes. Twenty states only specify live load models as opposed to specific legal vehicles. These live load models include:

- HS-20: three axle truck with a total gross weight of $72,000 \mathrm{lbs}$.
- HS-25: three-axle truck with axle loads $25 \%$ higher than HS-20, with a total gross weight of 90,000 lbs.
- HL-93: vehicle design load consisting of three parts: one, a three-axle truck with a total gross weight of 72,000 lbs.; two, a design tandem axle consisting of two axles spaced four feet apart with axle loads of 25,000 lbs. each; three, a design lane load of 0.64 kips per linear foot. The design force of HL-93 is either the three axle truck load plus the design lane load, or the design tandem axle plus the design lane load, whichever is greater.

| AL | 2 |
| :---: | :---: |
| AZ | 1 |
| AR | 1 |
| CA | 1 |
| CO | 1 |
| CN | 2 |
| DE | 8 |
| FL | 8 |
| GA | 1 |
| ID | 1 |
| IL | 2 |
| IN | 11 |


| IO | 1 |
| :---: | :---: |
| KA | 1 |
| KY | 6 |
| LA | 1 |
| ME | 1 |
| MD | 2 |
| MA | 4 |
| MI | 28 |
| MN | 7 |
| MS | 5 |
| MO | 1 |
| MT | 2 |


| NE | 3 |
| :---: | :---: |
| NV | 1 |
| NH | 1 |
| NJ | 4 |
| NM | 11 |
| NY | 1 |
| NC | 29 |
| ND | 1 |
| OH | 7 |
| OR | 4 |
| PA | 4 |


| RI | 1 |
| :---: | :---: |
| SC | 1 |
| SD | 4 |
| TX | 1 |
| UT | 14 |
| VT | 21 |
| VA | 4 |
| WA | 9 |
| WV | 5 |
| WI | 8 |
| WO | 1 |


| Key |  |
| :---: | :---: |
|  | 1 |
|  | $2-5$ |
|  | $6-10$ |
|  | $11-15$ |
|  | $16-25$ |
|  | $25+$ |

Figure 2.3: Current count of legal vehicles for states with publicly available data.


Figure 2.4: Comparison of state legal vehicle counts.

### 2.3 Vehicles that Exceed Federal Legal Loads

As described in section 2.2, there are three separate grandfather clauses in Title 23 USC§127. The 1956 grandfather clause relates principally to axle weights, gross weights, and permitting practices. The 1975 grandfather clause deals with bridge formula and axle spacing tables. Lastly, the 1991 grandfather clause codifies state practices relating to Longer Combination Vehicles (Fox, 2015). These clauses allow states flexibility in balancing the eventual degradation of roadway structures with the impact to local economies, freight movements, and traffic densities that can be positively impacted by allowing greater freedom of movement to overweight vehicles.

In addition to these grandfather clauses, states have specific exemptions for vehicles that exceed federal weight limits. These include grandfathered provisions to the axle weight limits and exemptions for specific vehicle types; these pertain to vehicles considered vital to local industry (vehicles hauling coal in Kentucky or West Virginia are
SEF. \#

Figure 2.5: North Carolina non-interstate legal vehicles
permitted to weigh up to $120,000 \mathrm{lbs}$.; trucks transporting lumber in California are allowed a maximum tandem axle load of $69,000 \mathrm{lbs}$.; trucks carrying cotton/seed in southern states such as North Carolina are allowed a maximum tandem axle load of $50,000 \mathrm{lbs}$. ), vehicles considered vital to infrastructure construction/rehabilitation (ready-mix concrete trucks,
trucks carrying construction materials or equipment), and vehicles considered vital to public health (garbage trucks, solid waste removal vehicles).

### 2.4 Influence Lines

Influence lines are spatial functions that represent the response of a structure at a fixed point due to a unit load at another (moving) point. For one dimensional skeletal structures, influence lines can be thought of as functions of the position $x$ of the unit load. The response of the structure usually involves a generalized displacement, and a generalized internal force at the point under consideration. For beam structures, the internal forces are typically the bending moment or the shear force, but influence lines for strains, stresses, or reactions at a point are also of common occurrence. The present study will concentrate on shear and bending moment influence lines. Influence lines have been around since the late nineteenth century, the first references dating from 1867 (Charlton, 1982).

For statically determinate structures such as simply supported beam structures, influence lines can be calculated directly using the principles of statics. They can also be determined using the principle of virtual work. Influence lines for statically determinate structures like simple beams consists of straight line segments.

Table 1: Legal Vehicles

| State | Legal Vehicles |
| :---: | :---: |
| Alabama | HS20-44, and Alternate PPM20-4, 8/10/56 for Interstates only |
| Alaska | No publicly available data |
| Arizona | HL-93 |
| Arkansas | HS20 |
| California | HL-93 |
| Colorado | HL-93 |
| Connecticut | HS20, HL-93 |
| Delaware | HL-93, HS 20-44, S220, S335, S437, T330, T435, and T540 |
| Florida | HL-93, SU2, SU3, SU4, ST5, C3, C4, C5 |
| Georgia | HL-93 |
| Hawaii | No vehicles/legal loads listed |
| Idaho | HL-93 |
| Illinois | IL-120, HL-93 |
| Indiana | HL-93; Legal loads R1, R2, R3; Permit Loads R4, R5, S1, S2, S3, S4, S5 |
| Iowa | HL-93 |
| Kansas | HL-93 |
| Kentucky | HL-93, HS20, Type 1 (H-truck), Type 2 (Tandem Truck), Type 3 (Tri-axle truck), Type 4 (Five-axle tractor-trailer) |
| Louisiana | HL-93 |
| Maine | HL-93, Legal Load Configurations 1-8 |
| Maryland | HL-93, HS20 |
| Massachusetts | H20, Type 3, Type 3S2, HS20 |
| Michigan | 28 legal vehicles |
| Minnesota | M3, M3S2-40, M3S3-40, SU4, SU5, SU6, SU7 |
| Mississippi | HS20, H-Truck, Concrete Truck, HS-Short, HS-Long |
| Missouri | HL-93 |
| Montana | HL-93, HS25 |
| Nebraska | Type 3, Type 3S2, Type 3-3 |
| Nevada | HL-93 |
| New <br> Hampshire | HL-93 |

Table 1: Legal Vehicles (cont'd)

| State | Legal Vehicles |
| :---: | :---: |
| New Jersey | HS20-36T, 3-25T, 3S2-40T, 3-3-40T |
| New Mexico | HS20, HL93, (1) two-axle load, (3) three-axle load, (1) four-axle load, (1) five-axle load, (3) six-axle load - (11) total |
| New York | HL-93 |
| North Carolina | SH, S3A, S3C, S4A, S5A, S6A, S7A, S7B, T4A, T5B, T6A, T7A, T7B, SNSH, SNGARBS2, SNAGRIS2, SNCOTTS3, SNAGGRS4, SNS5A, SNS6A, SNS7B, TNAGRIT3, TNT4A, TNAGRIT4, TNAGR5A, TNAGT5B, TNT6A, TNT7A, TNT7B |
| North Dakota | HL-93 |
| Ohio | 2F1, 3F1, 4F1, 5C1, HL-93, HS25, HS20-44 |
| Oklahoma | No publicly available data |
| Oregon | HL-93, OR-STP-4D, OR-STP-5BW, OR-STP-4E |
| Pennsylvania | PHL-93, Permit Load P-82, ML-80, TK527 |
| Rhode Island | HL-93 |
| South Carolina | HL-93 |
| South Dakota | HL-93, Type 3, Type 3S2, Type 3-2 |
| Tennessee | No publicly available data |
| Texas | HL-93 |
| Utah | HL-93, HS-20, Type 3, Type 3S2, Type 3-3, SU4, SU5, SU6, SU7, Permit vehicles UT-P6, UT-P7, UT P8, UTP9a, UT-P9b |
| Vermont | 3S2, 6 axle trailer, 3 axle straight, 4 axle straight, 5 axle semi, HS20, HL93 |
| Virginia | HL-93, HS-20, VA Type 3, VA Type 3S2 |
| Washington | HL-93, HS20, Type 3, Type 3S2, Type 3-3, NRL, Legal Lane, OL1 and OL2 |
| West Virginia | HL93, H, Type 3, WV-SU4, HS, 3S2. Bridges on a coal resource transportation system shall be load rated for WVSU40, WV-SU45, WV-3S55, WV-3S60 |
| Wisconsin | HL-93, Type 3, Type 3S2, Type 3-3, SU4, SU5, SU6, and SU7 |
| Wyoming | HL-93 |

For statically indeterminate structures like continuous beams, the calculation of influence lines is usually performed using the principle of virtual work in conjunction with Maxwell-Betti's Law of reciprocal displacements. This combination is known as MullerBreslau's Principle which also dates from the late $19^{\text {th }}$ century (Charlton, 1982).

Recent studies use influence lines in the areas of health monitoring of structures (Catbas e. al., 2012)), and to find the ultimate capacity of bridge structures under moving loads (Fiorillo et. al., 2015). Another recent study uses force-based finite elements to develop a procedure to analyze structures under moving loads that has proven useful for load rating of bridges (Kidarsa et. al., 2008). Figure 2.5 shows an influence line for bending moment of a single span constructed using Muller Breaslau's Principle; Figure 2.6 shows an influence line for bending moment at midspan of a 2 -span continuous beam.

Influence lines are used to identify the loading and loading configurations that produce the greatest effect on a structure. Several methods to developing influence lines for moving loads are discussed below.


Figure 2.6: Influence Line for Moving Vehicles, Two Consecutive Single Spans.


Figure 2.7: Influence Line for Moving Vehicles, Two Continuous Multiple Span.
In the first method, unit influence lines (UIL) are developed using computer images and sensor data. Influence lines are created by applying a unit load and moving it across the structure. The influence lines are generated by plotting the reactions to this unit load at a given location of interest. To generate this UIL, the following formula should be used (Zaurin, 2010):

$$
\{r\}=[w] *\{u\}
$$

Where:
$\{r\}$ is a vector containing the response of a given location resulting from the moving load,
[w] is a matrix of the axle weights, and $\{u\}$ is the UIL vector.

UIL can be calculated by rearranging the following equation:

$$
\{u\}=[w]^{-1} *\{r\}
$$

When using this formula, $\{r\}$ and $[w]$ are collected from the monitoring data as well as axle loads and locations and $[w]^{-1}$ is calculated using standard numerical techniques (Catbas, 2012).

This methodology was tested by creating a simulation of two remote controlled vehicles moving over an undamaged structure. The raw data collected from the simulation consists of a combination of a static response, a dynamic response, and noise. The dynamic response and noise must be filtered out from the static response by using a Fourier transformation that changes the time domain to frequency domain. The result from this filtering process is then converted back to the time domain. Through synchronized computer image data, the response of the structure is correlated with the corresponding input force and location. The UIL can then be calculated. Due to their ability to provide a more localized response, the UILs for strain could be used for instance to pinpoint damage to a structure (Zaurin, 2010).

A second method utilizes a nonlinear analysis of the bridge subjected to moving loads. The moment or shear at three critical locations are analyzed to obtain the influence lines for the structure. The three critical locations are labeled with the letters B, S, and C. The corresponding ultimate moment capacity and shear are labeled with $M_{u, B}, M_{u, S}, M_{u, C}$, and $V_{u, B}, V_{u, S,}, V_{u, C}$. The influence line for moment and shear are (Fiorillo, 2015):

$$
\begin{aligned}
& \lambda_{M, i}^{j}(x)=\sum_{k=1}^{R} \alpha_{k} * \lambda_{M, i}^{j}\left(X_{k}\right) \\
& \lambda_{V, i}^{j}(x)=\sum_{k=1}^{R} \alpha_{k} * \lambda_{V, i}^{j}\left(X_{k}\right)
\end{aligned}
$$

Where:
$i$ is the section
j is the j -th structural configuration
k is the k -th force out of R forces located at $X_{k}$ from the left origin $\alpha_{k}$ is the ratio between the force k and the maximum force in the set applied; $\alpha_{k}$ can assume a value between 0 and 1.

To test the methodology outlined above, the results were compared to the structural analysis program SAP2000 as well as the theoretical results from solving this problem using the principle of virtual work. There is a small discrepancy in the calculated results when compared to SAP2000. This is likely due to the nonlinear structural analysis software package which is commonly subject to numerical instability. The discrepancies are minimal enough and can be attributed to the software package rather than the proposed methodology to conclude that this methodology can be used. This approach is developed as an extension of the stiffness matrix, one of the most commonly used methods for solving structural analysis problems. In addition, this approach can identify critical loading positions when these positions are unknown and considers combinations of ductile or brittle section failures resulting from shear or bending moments (Fiorillo, 2015).

A third approach to developing influence lines for moving loads is the low-order approach. Two assumptions were made that formed the basis of this approach and they are "there will be a numerical integration error for any quadrature method" and "for the common case of a prismatic element without interior loads, the integration of quadratic polynomials is sufficient to represent the product of a linear curvature distribution" (Kidarsa, 2008). Because of these assumptions, three integration weights must be treated as unknown. The remaining weights ( $\mathrm{N}-3$ ) should be specified in order to maintain accuracy. The integration points are divided into groups depending on if the weight is known $\left(N_{c}\right)$ or unknown $\left(N_{f}\right)$. The following integration was then developed:

$$
\left[\begin{array}{cccc}
1 & 1 & \ldots & 1 \\
x_{f 1} & x_{f 2} & \ldots & x_{f N_{f}} \\
\vdots & \vdots & \ddots & \vdots \\
x_{f 1}^{N_{f}-1} & x_{f 2}^{N_{f}-1} & \ldots & x_{f N_{f}}^{N_{f}-1}
\end{array}\right] *\left[\begin{array}{c}
w_{f 1} \\
w_{f 2} \\
\vdots \\
w_{f N_{f}}
\end{array}\right]=\left[\begin{array}{c}
(b-a)-\sum_{j=1}^{N_{c}} w_{c j} \\
\left(b^{2}-a^{2}\right) / 2-\sum_{j=1}^{N_{c}} x_{c j} w_{c j} \\
\vdots \\
\left(b^{N_{f}}-a^{N_{f}}\right) / N_{f}-\sum_{j=1}^{N_{c}} x_{c j}^{N_{f}-1} w_{c j}
\end{array}\right]
$$

Where:
$x_{f}$ and $x_{c}$ are the integration point locations, their corresponding weights are $w_{f}$ and $w_{c}$, and $[\mathrm{a}, \mathrm{b}]$ is the interval of integration.

This method is suitable for both moving load analysis and for nonlinear material response over a set length (Kidarsa, 2008).

The low-order approach was applied to a moving load analysis of the McKenzie River Bridge near Eugene, OR. A three-axle AASHTO HS-20 truck was moved across the bridge. Integration weights were assigned to sections $1,2,6$, and 7 while sections $3-5$ were left unknown. The internal moment and shear demand resulting from the moving load are computed using one force-based beam element at each of the critical locations. The calculated moment and shear were compared to the actual values and the errors were small, concluding that this is an accurate and reliable approach. The results of this research are now used in load rating software developed for the Oregon Department of Transportation to efficiently rate state bridges (Kidarsa, 2008).

### 2.5 Determination of Live Load Envelopes

Prior to the development of federal standards for vehicle weight limits, equivalent uniform live load envelopes were developed in an effort to simplify and standardize bridge design. In this methodology, design moments and shears, equivalent uniform loads for moments, and equivalent uniform moments for shear were calculated for three classes of bridges. The bridge classes include: industrial bridges, pertaining to all spans normally carrying heavy trucking loads; route bridges, consisting of interstate and highway bridges experiencing normal interstate trucking loads; and rural bridges, consisting of lightly travelled structures that do not experience heavy truck loads. The results of this methodology is a series of live load envelopes, as opposed to single uniform loads (Schaffer, 1952).

In later research, live load distribution generated by oversized trucks was examined. In this research, modification factors were developed for girder distribution factors (GDF) for girder bridges subject to vehicles with a gauge larger than 6 feet, examining vehicles that would normally require a permit to use routes that included bridge crossings. Finiteelement modeling was utilized to determine shear GDF and flexural GDF for three different composite steel bridge structures. This analysis showed a reduction in GDF corresponding to an increase in gauge length, indicated that the first interior girder received the largest percentage of live load, and showed that gauge width affects shear more than it affects flexure (Tabish and Tabatabai, 2001).

In additional research, bridge rating when subjected to loads from military vehicles was investigated. In this investigation, the bridge response when subjected to loads from
military vehicles to those when the bridge was subjected to standard AASHTO HS20 trucks was compared. The study compared AASHTO's Load and Resistance Factor Rating (LRFR) rating equation with the rating equation specified in the Canadian Highway Bridge Code, as well as rating equations relating to military vehicles specifically proposed by Pinero (Pinero, 2001) and Ortiz (Ortiz, 2007). Four vehicles and six bridge models were tested; in examining the effects of the loads on each girder in the six bridge models, a total of 144 cases were considered. The study found that the wheel-line spacing of the military trucks contributed the highest factor to the distribution of the live load for all girders, interior or exterior. It further found the AASHTO LRFR provisions were adequate at predicting the load effect of the military trucks (Kim, et al, 2013).

### 2.6 Summary

The number of vehicles currently utilized by the NCDOT to load rate bridges is significantly higher than are used in most states. This list of vehicles can be optimized by determining the vehicles that control during the load rating process. Influence line analysis will be utilized to determine moment and shear envelopes for the vehicles. The moment and shear envelopes could subsequently be used to determine operating weights for the vehicles. The controlling vehicles will be the ones with the lowest operating weights. Applying this analysis to a variety of bridges will allow for the determination of the controlling vehicles. The resulting optimized list of vehicles will be populated by the vehicles found to control through this analysis.

# Chapter 3: Optimization of Legal Posting Vehicles 

### 3.1 Optimization Methodology

The optimization methodology began by duplicating the results obtained by NCDOT in bridge maintenance analysis. Sample analysis results were provided for four bridge spans. These include two timber beam bridges (bridge number 500225 and bridge number 480221) and two spans of one steel beam bridge (bridge number 490054). An examination of the methods used to determine the operating and inventory rating for the truck loads on the provided bridge spans is presented below.

Operating and inventory ratings are used to determine the operating and inventory weights for each vehicle used during the load rating process. Multiplying the gross weight of a vehicle by the operating rating yields the operating weight; multiplying the gross weight of a vehicle by the inventory rating yields the inventory weight. The inventory weight represents the vehicle load that can safely traverse the bridge frequently and repeatedly. The operating weight represents the maximum permissible vehicle load to which a bridge may be subjected; repeated exposure to vehicles at operating weight may shorten the life of the bridge. The operating rating also indicates whether the bridge must be posted for maximum vehicle loads. If a legal vehicle type has an operating rating at or above 1.0 , no posting for that vehicle is necessary; if the operating rating is below 1.0 , the
bridge must have a sign indicating the maximum inventory weight for that classification of vehicle.

The spans for bridge 490054 include a 19.75 ft . span and a 39.0 ft . span. Analysis for the 19.75 ft . span was performed on an interior W12x27 bean; analysis for the 39.0 ft . span was performed on an interior W16x50 beam. Relevant details for each span are as follows:

Table 2: Timber Span Analysis

|  | W12x27 | W16x50 |
| :---: | :---: | :---: |
| Percent effect | 98.0 | 98.0 |
| Yield stress ( $\mathrm{lb} / \mathrm{in}^{2}$ ) | 33000 | 33000 |
| Deck material | Timber | Timber |
| Beam spacing (ft) | 2.115 | 2.583 |
| Non-composite dead load ( $\mathrm{lb} / \mathrm{ft}$ ) | 134 | 179 |
| Impact + 1 | 1.3 | 1.3 |
| Reduced $\mathrm{S}_{\mathrm{x}}\left(\mathrm{in}^{3}\right)$ | 30.5923 | 58.1735 |

Due to the age of the bridge, the rating factor for the spans was determined with the load factor rating (LRF) formula:

$$
R F=\frac{C-A_{1} * D}{A_{2} * L * G D F *(1+I)}
$$

Where:

$$
\begin{aligned}
& \mathrm{RF}=\text { rating factor } \\
& \mathrm{C}=\text { capacity } \\
& \mathrm{A}_{1}=\text { dead load factor } \\
& \mathrm{D}=\text { dead load effect }
\end{aligned}
$$

$\mathrm{A}_{2}=$ live load factor
$\mathrm{L}=$ live load effect
GDF = girder distribution factor
$\mathrm{I}=$ impact
Girder distribution factor is used to account for the spacings of the girders. For steel girder bridges, GDF is determined with the following equation:

$$
G D F=\frac{\text { Beam Spacing }}{4}
$$

Where:

GDF $=$ girder distribution factor

Beam spacing $=$ distance between center of girders

Impact reflects the dynamic effects of moving loads on a bridge. Impact has a maximum value of 0.3 , and is determined with the following equation:

$$
I=\frac{50}{L+125}
$$

Where:

$$
\begin{aligned}
& I=\text { impact } \\
& L=\text { length of span }
\end{aligned}
$$

The dead and live load factors for the inventory and operating levels are listed below:

## Table 3: Live Load Factors

|  | $\mathrm{A}_{1}$ | $\mathrm{~A}_{2}$ |
| :--- | :--- | :--- |
| Inventory | 1.3 | 2.17 |
| Operating | 1.3 | 1.3 |

The difference between the two rating factors is the live load factor. The ratio between the Inventory rating and the operating rating is $3: 5$; this ratio is induced into the LRF formula by multiplying the live load factor used to determine the operating rating by $5 / 3$ when calculating the inventory rating.

Capacity is determined by multiplying the section modulus $\left(\mathrm{S}_{\mathrm{X}}\right)$ by the yield stress ( $\mathrm{F}_{\mathrm{Y}}$ ):

$$
C=S_{X} * F_{Y}
$$

The distribution factor for the live load effect for a bridge with one lane in either direction and a timber deck is found by dividing the beam spacing by four. This distribution factor represents one wheel line; doubling the distribution factor will return a rating factor for the axle load.

Using the appropriate dead and live load factors, rating factors for the operating and inventory level are calculated. The operating and inventory weights are then determined by multiplying the rating factor by the truck weight:

$$
\text { Operating Weight }=\text { Truck Weight } * R F
$$

For the sake of brevity, the demonstration of the process will focus on one specific truck load, that of the HS truck. Similarly, the demonstration will focus on the 39.0 ft . span, and concentrate on the operating rating and weight. Results obtained from this analysis
were found to be representative of all results obtained, for all truck loads, both spans, and both Operating and Inventory levels. The truck weight for an HS truck is 15.0 tons, and the Live Load moment for the HS truck on a 39.0 ft . span based on its axle load is 319.38 kip * ft.

The first step was to determine the target rating factor. This was merely a process of rewriting the Operating weight equation:

$$
R F=\frac{\text { Operating Weight }}{\text { Truck Weight }}
$$

The next step was to determine the component values to use in the LRF RF equation. The dead load moment was determined as such:

$$
D=\frac{w L^{2}}{8}=\frac{\left(179 \frac{\mathrm{lb}}{f t}\right) *(39 \mathrm{ft})^{2} * \frac{12 \mathrm{in}}{1 \mathrm{ft}} * \frac{1 \mathrm{kip}}{1000 \mathrm{lb}}}{8}=408.4 \mathrm{kip} * \mathrm{in}
$$

Capacity was determined by multiplying the reduced section modulus of the damaged $\mathrm{W} 16 \times 50$ beam by its yield stress:

$$
C=58.1735 \mathrm{in}^{3} * 33000 \frac{\mathrm{lb}}{i \mathrm{n}^{2}} * \frac{1 \mathrm{kip}}{1000 \mathrm{lb}}=1919.7 \mathrm{kip} * \mathrm{in}
$$

The live load moment was converted into kip * in, and halved to represent the wheel load:

$$
L=319.38 \mathrm{k} * \mathrm{ft} * 0.5 * \frac{12 \mathrm{in}}{1 \mathrm{ft}}=1916.3 \mathrm{kip} * \mathrm{in}
$$

The distribution factor for the span was obtained:

$$
D F=\frac{\text { Beam Spacing }}{4}=\frac{2.538}{4}=0.646
$$

The obtained results were entered into the RF equation:

$$
R F=\frac{C-A_{1} * D}{A_{2} * D F * L *(1+I)}=\frac{(1919.7 \text { kip } * \text { in })-(1.3) *(408.4 \text { kip } * \text { in })}{(1.3) *(0.646) *(1916.3 \text { kip } * \text { in }) *(1.3)}=0.664
$$

Applying this rating factor to the truck weight for the HS truck yields the following Operating Weight:

$$
\text { Operating Weight }=\text { Truck Weight } * R F=15 \text { tons } * 0.664=9.96 \text { tons }
$$

With a rating factor for a legal vehicle that is determined to be below 1.0 , this bridge would be weight restricted, and the need for that is apparent in the calculated operating weight. An HS truck operating at its maximum weight of 15 tons would not be able to cross this span without the risk of damaging the bridge. To prevent damage, the HS truck would be restricted to a total maximum gross weight of 9.96 tons.

### 3.2 Serviceability Check

The span was subsequently checked to determine whether the controlling factor in the bridge rating was strength or serviceability. The process for strength rating is as described above. The check for serviceability for non-composite sections is determined with the following equation:

$$
R F_{O}=\frac{0.80 F_{Y}-F_{D L}}{1.67 * F_{L L+1}}
$$

Where:

$$
\begin{aligned}
& \mathrm{RF}_{\mathrm{O}}=\text { operating rating factor } \\
& \mathrm{F}_{\mathrm{Y}}=\text { yield stress of member } \\
& \mathrm{F}_{\mathrm{DL}}=\text { total dead load stress }=\mathrm{M}_{\mathrm{DL}} / \mathrm{S}_{\mathrm{X}} \\
& \mathrm{~F}_{\mathrm{LL}+1}=\text { total live load stress }=\mathrm{M}_{\mathrm{LL}+1} / \mathrm{S}_{\mathrm{X}} \\
& \mathrm{M}_{\mathrm{LL}+1}=\mathrm{M}_{\mathrm{LL}} * \mathrm{DF} * 1+\mathrm{I}
\end{aligned}
$$

The dead load stress was calculated:

$$
F_{D L}=\frac{408.4 \mathrm{kip} * \text { in }}{58.1735 \mathrm{in}^{3}}=7.02 \frac{\mathrm{kip}}{\mathrm{in}^{2}}
$$

The total live load stress was determined:

$$
F_{L L+1}=\frac{1916.3 \mathrm{kip} * \mathrm{in} * 0.646 * 1.3}{58.1735 \mathrm{in}^{3}}=27.66 \frac{\mathrm{kip}}{\mathrm{in}^{2}}
$$

The obtained values for the stresses was subsequently used to determine the rating factor for serviceability:

$$
R F_{O}=\frac{\left(0.80 * 33 \frac{\mathrm{kip}}{\mathrm{in}^{2}}\right)-7.02 \frac{\mathrm{kip}}{\mathrm{in}^{2}}}{1.67 * 27.66 \frac{\mathrm{kip}}{\mathrm{in}^{2}}}=0.419
$$

Since the rating factor due to serviceability was lower than the rating factor due to strength, the serviceability was found to control for this span.

### 3.3 NC Legal Vehicles $\mathbf{M}_{\text {max }}$ Matrix

The maximum bending moment for each of the 29 legal vehicles was determined for bridge spans between $40^{\prime}$ and $200^{\prime}$, in $10^{\prime}$ intervals. For each vehicle, the centroid
distance was determined. Placing the line of action for the vehicle at a point between the centroid of the vehicle and the center axle of the vehicle provided the maximum bending moment for that vehicle at that span distance.

The centroid was found with the following formula:

$$
C=\frac{\sum\left(D_{A} * P_{A}\right)_{\text {left }}-\sum\left(D_{A} * P_{A}\right)_{\text {right }}}{W_{T}}
$$

Where:

$$
\begin{aligned}
& C=\text { centroid of the axle loads } \\
& D_{A}=\text { distance between axle and center of vehicle } \\
& \mathrm{P}_{\mathrm{A}}=\text { load on axle } \\
& \mathrm{W}_{T}=\text { total vehicle weight }
\end{aligned}
$$

As an example of this process, consider the HS-20 truck on a span 100 ft . long. The HS-20 has a front axle with an 8 kip load, a central axle 14 ft . behind the front axle with a 32 kip load, and a rear axle 14 ft . behind the central axle with a 32 kip load, as seen below in Figure 3.1:


Figure 3.1: Graphical representation of axle loads and geometry of HS-20.

The determination of the vehicle centroid, relative to the central axle, is shown
below:

$$
C=\frac{(14 f t * 32 K)-(14 f t * 8 k)}{72 k}=4.667 f t
$$

A positive value for the centroid places it to the left of the central axle. The line of action for the vehicle is placed between the centroid and the central axle, as seen below in Figure 3.2:


Figure 3.2: Line of action (in red) for HL-20 on a 100 ft . span bridge.

The maximum bending moment values were obtained by drawing shear and bending moment diagrams. These values were subsequently verified with the program MOVLOADS. These values were tabulated (Figures 3.1 and 3.2), and the minimum and maximum bending moments for each span length were identified. Minimum values were highlighted in beige, and maximum values were highlighted in green.

| Vehicle | Span (ft.) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | 120 |
| SNSH | 263.1 | 303.4 | 370.8 | 438.1 | 505.6 | 573.0 | 640.5 | 707.9 | 775.4 |
| SNGARBS2 | 292.8 | 391.2 | 490.1 | 589.3 | 688.7 | 788.2 | 887.8 | 987.5 | 1087.3 |
| SNAGRIS2 | 299.5 | 406.8 | 515.0 | 623.7 | 732.7 | 842.0 | 951.4 | 1060.9 | 1170.5 |
| SNCOTTS3 | 470.5 | 606.7 | 742.9 | 879.2 | 1015.4 | 1151.6 | 1287.9 | 1424.1 | 1560.3 |
| SNAGGRS4 | 528.2 | 702.2 | 876.3 | 1050.6 | 1225.0 | 1399.4 | 1573.9 | 1748.4 | 1922.9 |
| SNS5A | 539.5 | 717.2 | 894.9 | 1072.7 | 1250.4 | 1428.2 | 1605.9 | 1783.6 | 1961.4 |
| SNS6A | 570.1 | 769.4 | 968.9 | 1168.5 | 1368.1 | 1567.7 | 1767.4 | 1967.1 | 2166.8 |
| SNS7B | 595.5 | 805.8 | 1015.8 | 1225.8 | 1435.8 | 1645.8 | 1855.8 | 2065.8 | 2275.8 |
| TNAGRIT3 | 462.0 | 627.0 | 792.0 | 957.0 | 1122.0 | 1287.0 | 1452.0 | 1617.0 | 1782.0 |
| TNT4A | 461.9 | 626.2 | 790.8 | 955.7 | 1120.6 | 1285.7 | 1450.8 | 1616.0 | 1781.2 |
| TNAGRIT4 | 535.1 | 749.1 | 963.4 | 1177.9 | 1392.5 | 1607.3 | 1822.0 | 2036.8 | 2251.7 |
| TNAGT5A | 572.5 | 797.4 | 1022.3 | 1247.3 | 1472.2 | 1697.2 | 1922.2 | 2147.2 | 2372.2 |
| TNAGT5B | 594.3 | 818.0 | 1042.2 | 1266.6 | 1491.1 | 1715.8 | 1940.5 | 2165.3 | 2390.1 |
| TNT6A | 540.6 | 748.3 | 956.2 | 1164.1 | 1372.0 | 1579.9 | 1787.9 | 1995.8 | 2203.8 |
| TNT7A | 531.6 | 740.7 | 950.0 | 1159.6 | 1369.2 | 1579.0 | 1788.7 | 1998.6 | 2208.4 |
| TNT7B | 519.6 | 716.8 | 920.7 | 1128.7 | 1337.1 | 1545.9 | 1755.0 | 1964.2 | 2173.5 |
| Span (ft.) |  |  |  |  |  |  |  |  |  |
| Vehicle | 130 | 140 | 150 | 160 | 170 | 180 | 190 | 200 |  |
| SNSH | 842.8 | 910.3 | 977.8 | 1045.3 | 1112.8 | 1180.3 | 1247.7 | 1315.2 |  |
| SNGARBS2 | 1187.1 | 1286.9 | 1386.7 | 1486.6 | 1586.5 | 1686.4 | 1786.3 | 1886.2 |  |
| SNAGRIS2 | 1280.1 | 1389.9 | 1499.6 | 1609.4 | 1719.2 | 1829.0 | 1938.8 | 2048.7 |  |
| SNCOTTS3 | 1696.6 | 1832.8 | 1969.1 | 2105.3 | 2241.6 | 2377.8 | 2514.1 | 2650.3 |  |
| SNAGGRS4 | 2097.5 | 2272.0 | 2446.6 | 2621.2 | 2795.7 | 2970.3 | 3144.9 | 3319.5 |  |
| SNS5A | 2139.1 | 2316.9 | 2494.6 | 2672.4 | 2850.1 | 3027.9 | 3205.6 | 3383.4 |  |
| SNS6A | 2366.5 | 2566.2 | 2765.9 | 2965.6 | 3165.3 | 3365.1 | 3564.8 | 3764.5 |  |
| SNS7B | 2485.8 | 2695.8 | 2905.8 | 3115.8 | 3325.8 | 3535.8 | 3745.8 | 3955.8 |  |
| TNAGRIT3 | 1947.0 | 2112.0 | 2277.0 | 2442.0 | 2607.0 | 2772.0 | 2937.0 | 3102.0 |  |
| TNT4A | 1946.5 | 2111.7 | 2277.0 | 2442.3 | 2607.6 | 2772.9 | 2938.2 | 3103.5 |  |
| TNAGRIT4 | 2466.6 | 2681.4 | 2896.4 | 3111.3 | 3326.2 | 3541.1 | 3756.1 | 3971.0 |  |
| TNAGT5A | 2597.2 | 2822.1 | 3047.1 | 3272.1 | 3497.1 | 3722.1 | 3947.1 | 4172.1 |  |
| TNAGT5B | 2614.9 | 2839.8 | 3064.7 | 3289.6 | 3514.5 | 3739.4 | 3964.3 | 4189.3 |  |
| TNT6A | 2411.8 | 2619.7 | 2827.7 | 3035.7 | 3243.7 | 3451.7 | 3659.6 | 3867.6 |  |
| TNT7A | 2418.3 | 2628.2 | 2838.1 | 3048.0 | 3257.9 | 3467.9 | 3677.8 | 3887.8 |  |
| TNT7B | 2383.0 | 2592.5 | 2802.1 | 3011.7 | 3221.4 | 3431.1 | 3640.9 | 3850.6 |  |

Figure 3.3: $\mathbf{M}_{\text {max }}$ matrix, non-interstate vehicles.
For the non-interstate trucks, the smallest maximum bending moments all occurred with vehicle SNSH. The largest maximum bending moment at 40 ft . was SNS7B; for all spans between 50 ft . and 200 ft ., the largest maximum bending moment was TNAGT5B.

|  | Span (ft) |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vehicle | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | 120 |
| SH | 216.2 | 278.5 | 340.8 | 403.2 | 465.6 | 528.0 | 590.5 | 652.9 | 715.4 |
| S3A | 383.3 | 497.0 | 610.8 | 724.5 | 838.3 | 952.0 | 1065.8 | 1179.5 | 1293.3 |
| S3C | 364.6 | 472.1 | 579.5 | 687.0 | 794.5 | 902.0 | 1009.5 | 1117.0 | 1224.5 |
| S4A | 415.2 | 548.7 | 682.4 | 816.0 | 949.7 | 1083.4 | 1217.1 | 1350.8 | 1484.6 |
| S5A | 464.7 | 617.2 | 769.6 | 922.1 | 1074.6 | 1227.1 | 1379.6 | 1532.1 | 1684.6 |
| S6A | 493.6 | 665.7 | 838.0 | 1010.3 | 1182.7 | 1355.1 | 1527.5 | 1700.0 | 1872.4 |
| S7A | 508.5 | 708.5 | 908.5 | 1108.4 | 1308.4 | 1508.4 | 1708.4 | 1908.4 | 2108.4 |
| S7B | 526.5 | 719.0 | 911.5 | 1104.0 | 1296.5 | 1489.0 | 1681.5 | 1874.0 | 2066.5 |
| T4A | 398.2 | 538.7 | 679.4 | 820.3 | 961.2 | 1102.3 | 1243.3 | 1384.4 | 1525.6 |
| T5B | 452.8 | 612.7 | 772.7 | 932.7 | 1092.6 | 1252.6 | 1412.6 | 1572.6 | 1732.6 |
| T6A | 468.6 | 648.5 | 828.4 | 1008.4 | 1188.3 | 1368.3 | 1548.3 | 1728.2 | 1908.2 |
| T7A | 477.2 | 677.2 | 877.2 | 1077.1 | 1277.1 | 1477.1 | 1677.1 | 1877.1 | 2077.1 |
| T7B | 442.0 | 613.2 | 805.1 | 1001.6 | 1198.9 | 1396.9 | 1595.2 | 1793.9 | 1992.8 |
|  |  |  |  | Span $(\mathrm{ft})$ |  |  |  |  |  |
| Vehicle | 130 | 140 | 150 | 160 | 170 | 180 | 190 | 200 |  |
| SH | 777.9 | 840.4 | 902.8 | 965.3 | 1027.8 | 1090.3 | 1152.8 | 1215.2 |  |
| S3A | 1407.0 | 1520.8 | 1634.5 | 1748.3 | 1862.0 | 1975.8 | 2089.5 | 2203.3 |  |
| S3C | 1332.0 | 1439.5 | 1547.0 | 1654.5 | 1762.0 | 1869.5 | 1977.0 | 2084.5 |  |
| S4A | 1618.3 | 1752.0 | 1885.8 | 2019.5 | 2153.2 | 2287.0 | 2420.7 | 2554.4 |  |
| S5A | 1837.1 | 1989.6 | 2142.1 | 2294.5 | 2447.0 | 2599.5 | 2752.0 | 2904.5 |  |
| S6A | 2044.9 | 2217.3 | 2389.8 | 2562.3 | 2734.7 | 2907.2 | 3079.7 | 3252.2 |  |
| S7A | 2308.4 | 2508.4 | 2708.4 | 2908.4 | 3108.4 | 3308.4 | 3508.4 | 3708.4 |  |
| S7B | 2259.0 | 2451.5 | 2644.0 | 2836.5 | 3029.0 | 3221.5 | 3414.0 | 3606.5 |  |
| T4A | 1666.7 | 1807.9 | 1949.1 | 2090.2 | 2231.4 | 2372.6 | 2513.8 | 2655.0 |  |
| T5B | 1892.6 | 2052.6 | 2212.6 | 2372.6 | 2532.6 | 2692.6 | 2852.6 | 3012.6 |  |
| T6A | 2088.2 | 2268.2 | 2448.2 | 2628.2 | 2808.2 | 2988.1 | 3168.1 | 3348.1 | 3677.0 |

Figure 3.4: $\mathbf{M}_{\text {max }}$ matrix, interstate vehicles.
For the interstate trucks, the smallest maximum bending moments all occurred with vehicle SH . The largest maximum bending moment from 40 ft . to 60 ft . was S 7 B ; for all spans between 70 ft . and 200 ft ., the largest maximum bending moment was S7A.

### 3.4 NCDOT Bridge Analysis

In addition to the initial sample analysis of the four spans, NCDOT provided analysis data of 18 additional bridges. The controlling factor for most of the provided
bridges was Serviceability; Strength was the controlling factor for two bridges (bridge \# 770056 and bridge \# 900028). The provided data was analyzed for two purposes:

1. To determine the total number of controlling vehicles.
2. To determine whether the same Rating Factor values that were obtained by NCDOT could be calculated for bridges where strength was the controlling factor.

The data provided for bridge 770056 was entered into a spreadsheet, and $\mathrm{RF}_{\mathrm{O}}$ and $\mathrm{RF}_{\mathrm{I}}$ were calculated for all 16 non-interstate trucks at varying levels of bridge effectiveness and varying levels of section modulus. Effectiveness was calculated beginning at $100 \%$, and for all values declining by $1 \%$ until $90 \%$ effectiveness was reached. Section modulus was calculated beginning at $100 \%$, and for all values declining by $5 \%$ until $70 \%$ was reached; additionally, a value for section modulus at $50 \%$ was also calculated. Each level of effectiveness was calculated for each level of section modulus; in total, $88 \mathrm{RFo}_{\mathrm{o}}$ and $\mathrm{RF}_{\mathrm{I}}$ values were calculated for all 16 vehicles (Figure 3.5).

The controlling vehicle for each combined set of conditions was the vehicle with the lowest value for operating weight (disregarding the notional vehicle HS). For bridge 770056, in all combined set of conditions, SNSH was determined to be the controlling vehicle (Figure 3.6).


Figure 3.5: $\mathbf{R F}_{\mathbf{0}}$ and $\mathbf{R F}_{\mathrm{i}}$ values calculated for bridge $\mathbf{7 7 0 0 5 6}$ at $\mathbf{1 0 0 \%}$ section modulus and $100 \%$ effectiveness.

Furthermore, when SNSH was removed from consideration, the controlling vehicle for all combined sets of conditions was found to be SNCOTTS3. At all levels of effectiveness between $90 \%$ and $100 \%$, and all levels of section modulus between $70 \%$ and $100 \%$, SNSH had the lowest operating weight, and SNCOTTS3 had the second-lowest operating weight.

|  |  | Bridge Efficiency |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 99 | 98 | 97 | 96 | 95 | 94 | 93 | 92 | 91 | 90 |
|  | 100 | $\begin{gathered} \text { SNSH } \\ 31.3 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 30.9 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 30.6 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 30.2 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 29.8 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 29.4 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 29.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 28.7 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 28.3 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 27.9 \\ \hline \end{gathered}$ | SNSH <br> 27.5 |
|  | 95 | $\begin{gathered} \text { SNSH } \\ 29.4 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 29.1 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 28.7 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 28.3 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 28.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 27.6 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 27.2 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 26.9 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 26.5 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 26.2 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 25.8 \end{gathered}$ |
|  | 90 | $\begin{gathered} \text { SNSH } \\ 27.5 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 27.2 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 26.8 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 26.5 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 26.1 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 25.8 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 25.5 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 25.1 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 24.8 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 24.4 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 24.1 \\ \hline \end{gathered}$ |
| 左 | 85 | $\begin{gathered} \text { SNSH } \\ 25.6 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 25.3 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 25.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 24.6 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 24.3 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 24.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 23.7 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 23.3 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 23.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 22.7 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 22.4 \\ \hline \end{gathered}$ |
| تِّ | 80 | $\begin{gathered} \text { SNSH } \\ 23.7 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 23.4 \\ \hline \end{gathered}$ | SNSH <br> 23.1 | $\begin{gathered} \text { SNSH } \\ 22.8 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 22.5 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 22.2 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 21.9 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 21.6 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 21.3 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 21.0 \\ \hline \end{gathered}$ | SNSH $20.7$ |
|  | 75 | $\begin{gathered} \text { SNSH } \\ 21.8 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 21.5 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 21.2 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 20.9 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 20.7 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 20.4 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 20.1 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 19.8 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 19.5 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 19.2 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 18.9 \\ \hline \end{gathered}$ |
|  | 70 | $\begin{gathered} \text { SNSH } \\ 19.9 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 19.6 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 19.4 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 19.1 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 18.8 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 18.6 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 18.3 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { SNSH } \\ 18.0 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { SNSH } \\ 17.8 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 17.5 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 17.2 \\ \hline \end{gathered}$ |
|  | 50 | $\begin{gathered} \text { SNSH } \\ 12.3 \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 12.1 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 11.9 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 11.7 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 11.5 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 11.3 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 11.1 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 10.9 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 10.7 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 10.6 \\ \hline \end{gathered}$ | $\begin{gathered} \text { SNSH } \\ 10.4 \\ \hline \end{gathered}$ |

Figure 3.6: Controlling vehicle for all combined set of conditions on bridge \# 770056, and their respective operating weights (measured in tons).

This analysis was subsequently conducted on bridge \#320006, one of the 16 bridges provided by NCDOT where Serviceability was the controlling factor. SNSH was found to be the controlling vehicle in all combined sets of conditions, with SNCOTTS3 controlling once SNSH was removed from consideration.

The analysis provided by NCDOT for bridge \#770056 indicated a bridge at $98 \%$ effectiveness, with a section modulus value of $85.3111 \mathrm{in}^{3}$. The results obtained for the operating and inventory weights of trucks at that combined set of conditions is very similar to the results provided by NCDOT (Figure 3.5).

### 3.5 Optimized Load Critical Vehicles

28 steel girder bridges were tested in NCDOTs Wearable Inspection and Grading Information Network System (WGINS). Group 1 bridges consisted of sixteen bridges tested at varying levels of percent effectiveness and section modulus loss; group 2 bridges consisted of the twelve bridges tested at varying levels of percent effectiveness. The results of these tests were compiled to determine what effect the degradation of these bridge characteristics had on the posting vehicle for the bridge.

The rating factor for a vehicle is determined by dividing the operating/inventory weight by the gross vehicle weight. If any of the sixteen test vehicles returns an operating rating factor below 1.0, that bridge is determined to be weight restricted. The posting vehicle for a bridge is the vehicle with the lowest operating weight among the vehicles with an operating rating factor below 1.0.

Bridge effectiveness is listed in the bridge report as a percentage. This value is determined through subjective judgement by an NCDOT analyst based on the findings of a bridge inspection group. Section modulus refers to that value for the controlling steel girder of the bridge. This value cannot be directly adjusted in WIGINS, so the crosssectional area of the girder was adjusted until the target section modulus value was obtained. WIGINS permits adjusting the percent effectiveness for most steel girder bridges but does not permit the user to adjust beam characteristics for bridges where the steel girder

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION - BRIDGB MAINTENANCE
ANALYSIS SECTION

| Bridge Number: | 080037 | Date Of Rating: | $09-21-2017$ |
| :--- | :---: | :---: | ---: |
| County: | BLADEN | Rated By: | WIGINS |
| Date Of Inspection: $09-21-2017$ | Checked By: | null |  |
| Roadway Width(Inspection) :33.4 | Deck Out to Out : | 36.5 |  |


| Truck | Weight tons | Oper |  | $\begin{aligned} & \text { ry LLmom } \\ & \mathrm{K}-\mathrm{ft} \end{aligned}$ | nt Section | Controls |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HS | 15.00 | 36.2 | 21.7 | 290.80 | Compact | Serviceability |
| SNSH | 13.50 | 44.4 | 26.6 | 212.62 | Compact | Serviceability |
| SNGARBS2 | 20.00 | 54.3 | 32.6 | 258.64 | Compact | Serviceability |
| SNAGRIS2 | 22.00 | 59.1 | 35.5 | 262.27 | Compact | Serviceability |
| SNCOTTS3 | 27.25 | 45.0 | 27.0 | 422.88 | Compact | Serviceability |
| SNAGGRS4 | 34.92 | 52.2 | 31.3 | 467.43 | Compact | Serviceability |
| SNS5A | 35.55 | 52.0 | 31.2 | 477.29 | Compact | Serviceability |
| SNS6A | 39.95 | 55.8 | 33.5 | 500.33 | Compact | Serviceability |
| SNS7B | 42.00 | 56.1 | 33.7 | 522.35 | Compact | Serviceability |
| TNAGRIT3 | 33.00 | 57.0 | 34.2 | 404.25 | Compact | Serviceability |
| TNT4A | 33.08 | 57.2 | 34.3 | 404.57 | Compact | Serviceability |
| TNT6A | 41.60 | 62.1 | 37.3 | 467.89 | Compact | Serviceability |
| TNT7A | 42.00 | 64.0 | 38.4 | 459.78 | Compact | Serviceability |
| TNT7B | 42.00 | 64.5 | 38.7 | 455.11 | Compact | Serviceability |
| TNAGRIT4 | 43.00 | 65.3 | 39.2 | 460.30 | Compact | Serviceability |
| TNAGT5A | 45.00 | 63.6 | 38.2 | 493.79 | Compact | Serviceability |
| TNAGT5B | 45.00 | 61.0 | 36.6 | 516.10 | Compact | Serviceability |

Non-Interstate Traffic
Component: I-beam I-Bm Input:
Target Beam: Interior


Figure 3.7: WIGINS bridge analysis output for bridge \#080037 at $\mathbf{1 0 0 \%}$ effectiveness and $100 \%$ section modulus.
was reinforced with steel plates. As a result, group 1 bridges were tested at declining values of percent effectiveness and section modulus loss, and group 2 bridges were tested only for declining values of percent effectiveness. Section modulus was tested initially at $100 \%$; subsequent tests were made at declining intervals of $5 \%$, with the final test occurring at $70 \%$. For group 1 bridges, effectiveness was initially tested at $100 \%$; subsequent tests were made at declining intervals of $1 \%$, with the final test occurring at $90 \%$. For group 2 bridges, effectiveness was initially tested at the highest remaining value that resulted in all 16 vehicles receiving a rating factor of 1.0 or greater; subsequent tests were made at declining intervals of $1 \%$, with the final test occurring once the rating factor for SNCOTTS3 fell below 1.0. Group 1 bridges ranged in span length from 19.5 feet to 56.9 feet. Group 2 bridges ranged in span length from 50.8 feet to 162.9 feet. Group 2 bridges were included, despite the user's inability to adjust the section modulus, to examine the effect of effectiveness loss on larger bridge spans.

### 3.6 Summary

Three methodologies were developed to optimize the list of legal vehicles used by NCDOT to load rate non-interstate bridges. The maximum moment analysis showed that the vehicles providing the smallest maximum bending moments were SNSH (noninterstate vehicles) and SH (interstate vehicles). For shorter spans, the vehicles providing the largest maximum bending moments were SNS7B (non-interstate vehicles) and S7B (interstate vehicles); for longer spans, the vehicles providing the largest maximum bending moments were TNAGT5B (non-interstate vehicles) and S7A (interstate vehicles). The

NCDOT bridge analysis showed that SNSH controlled in all tested conditions. The optimized load critical vehicle method was found to be the most effective at determining the controlling posting vehicles; results of this methodology are presented in Chapter 5.

## Chapter 4: Automated Computer Program

### 4.1 Introduction

This computer program is designed to create possible truck configurations for varying axle combinations with varying lengths between the axles as allowed by the North Carolina Statutory Weights of Legal Vehicles as outlined in NC general statute § 20-118 (b)(3), and the Federal Bridge Formula. By imputing the North Carolina statutes distance and weights matrix and four axle distances, the program will generate possible truck combinations allowed by the statues. The following information will detail how to use the program and explain its outputs.

This computer program consists of three components:

- User Input File
- NC Statute Matrix
- Legal Truck Generation Program

The User Input File and NC Statute Matrix are text files, and the Legal Truck Generation Program is a program file written in the C programming language. The Legal Truck Generation Program reads the two text files and outputs a fourth component, the Truck Output File. This output file is a text file containing the trucks generated by the program, based on the parameters included in the input files.


Figure 4.1: Legal truck generation program process visualization.

### 4.2 User Input File

The User Input File (ncst_in.txt) permits the user to define the output parameters of the truck program. This text file consists of six sections. In the first section, the user specifies which trucks will be in the output file through the use of a Boolean operator, as seen in Figure 4.2:

```
Single Vehicles
2 1
3 1
4 1
50
60
70
Tractor Trailers
30
4 0
5 1
6 1
71
```

Figure 4.2: User truck selection.

This section has two columns. The left column corresponds to the number of axles on the truck, and the right column is the Boolean operator for that truck type. If a truck axle combination has a value of 1 , it will be included in the output file; if the value is zero, that truck combination will not be included in the output file. Running the truck program with an input file as shown in Figure 4.2 will return results for single vehicles with 2, 3, and 4 axles, and tandem trucks with 5, 6, and 7 axles.

The second section of the user input file gives the user the ability to dictate which formula will be used to generate the maximum legal weight for the trucks in the output file, as shown below in Figure 4.3. When a 1 is entered in this section, the maximum weight will be determined using the NC general statute; when a 0 is entered, the maximum weight will be determined using the Federal Bridge Formula.

```
Determination of Maximum Legal Weight. 1: NC statute; 0: Federal Bridge Formula (FBF)
1
```


## Figure 4.3: Maximum gross weight calculation.

The third section permits the user to generate a range of axle combinations for each truck axle type. This is controlled with a single parameter in this section. If this parameter is equal to 1 , a small number of axle combinations (termed "reduced") will be generated. If this parameter is equal to 2 , an intermediate number of axle combinations will be generated, and if the parameter is equal to 3 , a large number of axle combinations will be generated. The number of trucks generated by the program also depends on the number of axles, and on whether the truck is a single vehicle or a tractor trailer. In its present form, the number of trucks generated by the program for each number of axles ranges from 3 (for
single vehicle 2-axle configurations) to 1128 (for 7 -axle tractor trailers with the "large" axle combination option).

The fourth section permits the user to specify a maximum truck weight corresponding to an exception (e.g., a weight that is not in the statute matrix) and a minimum truck length to apply the exception.

The fifth section of the user input file allows the user to specify the truck axle spacings that will be used to generate the trucks in the output file. There is a maximum of four different distances for each truck ( $a, b, c, d$ ). Distances should be entered in terms of feet where ' $a$ ' is the smallest value, and values increase to ' $d$ ', the largest value. A different set of distances can be set for each truck type. These values can be changed by the user; however, it is important that the values are entered in ascending order, and that the smallest distance value corresponds to the distance between the axles in a tandem axle.

```
Specified distances between axles - SINGLE VEHICLE 2-axles
Number of distances
4
Actual distances
4.0 9.0 11.0 14.0
```

Figure 4.4: Sample axle spacings, single vehicle, two axles.


Figure 4.5: Truck axle spacing diagram with $\mathbf{a} / \mathbf{b} / \mathbf{c}$ distances.


Figure 4.6: Truck axle spacing diagram with $\mathbf{a} / \mathbf{b} / \mathbf{d}$ distances.

Actual axle spacings and total truck length will be based on the values entered in the fifth section. Potential axle spacings, based on the $\mathrm{a} / \mathrm{b} / \mathrm{c} / \mathrm{d}$ values, will remain constant; the variety of potential spacings will be based on the user selection of the "reduced," "intermediate," or "large" output file. An example of axle combinations for a reduced output of five axle tandem trucks is presented below in Figure 4.7.

Five-axle tandem truck configuration 1:

Potential distance values:

| baba | caca | cada |
| :--- | :--- | :--- |
| baca | bada | daca |
| caba | daba | dada |

Five-axle tandem truck configuration 2:


Potential distance values:

| bbaa | ccaa | cdaa |
| :---: | :---: | :---: |
| cbaa | bdaa | dcaa |
| bcaa | dbaa | ddaa |

Figure 4.7: Example of axle combinations with distance values for a reduced output of five-axle tandem trucks.

The sixth section permits the user to enter the value for the bridge span used in the maximum bending moment calculations. This value is used by the program to calculate the maximum bending moment value for each generated vehicle.

The program utilized the influence line method to generate the maximum bending moment value for each generated vehicle at the user-specified span length. This method places one of the interior vehicle axles at the center of the span (Figure 4.8).

In the example presented in Figure 4.8 below, the five-axle truck has the axle distance combination of "b a c a." According to the values in Figure 4.4, that represents spacings of 9 feet, 4 feet, 11 feet, and 4 feet, respectively. The length of the center influence
line (originating at axle three and moving down to the x -axis) has a length equal to half of the span; for a 100 ft . span, the center influence line would represent 50 feet. The influence lines for the other axles have a length equal to half the span minus the distance between the specific axle and the center axle. For example, the influence line for A 1 would have a length of 37 feet $\left(50^{\prime}-4^{\prime}-9^{\prime}=37^{\prime}\right)$. The bending moment for this vehicle would be calculated by multiplying the axle loads by the length of their influence lines and summing the totals.


Figure 4.8: Graphic representation of influence line method of generating maximum
bending moment.

Due to the variety of possible truck geometries, the program calculates multiple bending moments for tandem trucks with five or more axles. One calculation is made by placing axle 3 at midspan, and another is made by placing axle 4 at midspan. The program compares the results and returns the largest possible bending moment in the output file. This process is illustrated in the logic diagram presented below in Figure 4.9:


Figure 4.9: Maximum bending moment calculation logic diagram.

The coding language used to execute this process is shown below in Figure 4.10. The first maximum bending moment calculation begins on line 3870 with the third axle located at midspan, and follows the process shown in Figure 4.8 above. The second maximum bending moment calculation begins on line 3882 ; for this calculation, the fourth axle (Ax4 in Figure 4.8) is placed at midspan. Comparison of the two values occurs in lines 3894 through 3897.


Figure 4.10: Excerpt of truck program code that executes the maximum bending moment calculation.

### 4.3 NC Statute Matrix

The NC Statute Matrix (statute_weights.txt) consists of the matrix of maximum truck gross weight based on axle count and truck length found in NC §20-118 (b)(3), as shown in Figure 4.11.

The axles column in the statute matrix represents the distance between the front and rear axles of the truck. The matrix text file utilizes the value of -1 to represent a blank value, as a value of 0 would be included in the calculations, whereas a negative value would not.

| Axles* | 2 Axles | 3 Axles | 4 Axles | 5 Axles | 6 Axles | 7 Axles | Distance - weignte matrix |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{4}$ | $38000$ |  | 4 Axies | SAxles | 6 Axies | 7 Axies | $0.020000 .0-2.0-2.0-1.0-2.0-2.0$ |
| 5 | 38000 |  |  |  |  |  | $1.020000 .0-1.0-1.0-1.0-1.0-1.0$ |
| 6 | 38000 |  |  |  |  |  | 2.0 20000.0-1.0 -1.0-1.0 -1.0 -1.0 |
| 7 | 38000 |  |  |  |  |  | $3.020000 .0-1.0-2.0-1.0-2.0-1.0$ |
| 8 or |  |  |  |  |  |  | $4.038000 .0-1.0-1.0-1.0-1.0-1.0$ |
| less | 38000 | 38000 |  |  |  |  | $5.038000 .00^{-1}-1-1-1-1-1$ |
| more |  |  |  |  |  |  | 7.0 38000.0-1 -1 -1 -1-1 |
| than 8 | 38000 | 42000 |  |  |  |  | 7.538000 .0 38000.0-1-1 -1-1 |
| 9 | 39000 | 42500 |  |  |  |  | $1.038000 .038000 .0-1-1-1-1$ |
| 10 | 40000 | 43500 |  |  |  |  | $8.538000 .042000 .0-1-1-1$ |
| 11 |  | 44000 |  |  |  |  | $5.035000 .042500 .0-1-1-1$ |
| 12 |  | 45000 | 50000 |  |  |  | $104000043500-1-2-1-1$ |
| 13 |  | 45500 | 50500 |  |  |  | $11-1440000^{-1}-1-1-1$ |
| 14 |  | 46500 | 51500 |  |  |  | $12-14500030000-1-1-1$ |
| 15 |  | 47000 | 52000 |  |  |  | $13-14850080800-1-1-1$ |
| 16 |  | 48000 | 52500 | 58000 |  |  | $14-14650051500-1-1-1$ |
| 17 |  | 48500 | 53500 | 58500 |  |  | $15-14700052000-1-1-1$ |
| 18 |  | 49500 | 54000 | 59000 |  |  | 16-1 $480005250058000-1-1$ |
| 19 |  | 50000 | 54500 | 60000 |  |  | ${ }^{17}$-1 $4835008350083800-1-1$ |
| 20 |  | 51000 | 55500 | 60500 | 66000 |  | 18 -1 $495008500085000-1-1$ |
| 21 |  | 51500 | 56000 | 61000 | 66500 |  | $19-1500008450060000-1-1$ |
| 22 |  | 52500 | 56500 | 61500 | 67000 |  | -1 $51000355006050066000-$ |
| 23 |  | 53000 | 57500 | 62500 | 68000 |  | $22-15250056000681200066500-1$ |
| 24 |  | 54000 | 58000 | 63000 | 68500 | 74000 | -1 $523008650006150067000-1$ |
| 25 |  | 54500 | 58500 | 63500 | 69000 | 74500 | ${ }^{-1} 530005750062500688000-1$ |
| 26 |  | 55500 | 59500 | 64000 | 69500 | 75000 |  |
| 27 |  | 56000 | 60000 | 65000 | 70000 | 75500 | 26-1 $55500555500 \times 600006550975090$ |
| 28 |  | 57000 | 60500 | 65500 | 71000 | 76500 |  |
| 29 |  | 57500 | 61500 | 66000 | 71500 | 77000 | $28-157000605006555007100076500$ |
| 30 |  | 58500 | 62000 | 66500 | 72000 | 77500 | 29-1 575006150066000071500077000 |
| 31 |  | 59000 | 62500 | 67500 | 72500 | 78000 |  |
| 32 |  | 60000 | 63500 | 68000 | 73000 | 78500 | $31-1590006250067500725007^{7} 8000$ |
| 33 |  |  | 64000 | 68500 | 74000 | 79000 |  |
| 34 |  |  | 64500 | 69000 | 74500 | 80000 | $33{ }^{-1}$-1 646000685007400079000 |
| 35 |  |  | 65500 | 70000 | 75000 |  | 34-1-1 6450006900074500880000 |
| 36 |  |  | $66000^{* *}$ | 70500 | 75500 |  | $35-1-1655007000075000-1$ |
| 37 |  |  | $66500^{* *}$ | 71000 | 76000 |  |  |
| 38 |  |  | $67500^{* *}$ | 72000 | 77000 |  | 37-1-167939 71000 76000-1 |
| 39 |  |  | 68000 | 72500 | 77500 |  | $38-1-1675357200077000-1$ |
| 40 |  |  | 68500 | 73000 | 78000 |  |  |
| 41 |  |  | 69500 | 73500 | 78500 |  | $40-1-1605007300078000-1$ |
| 42 |  |  | 70000 | 74000 | 79000 |  |  |
| 43 |  |  | 70500 | 75000 | 80000 |  | $42-1-1700007400079000-1$ |
| 44 |  |  | 71500 | 75500 |  |  | $43^{-1}-17050007500080000-1$ |
| 45 |  |  | 72000 | 76000 |  |  | $44^{-1}-1-1715007535000^{-1}-1$ |
| 46 |  |  | 72500 | 76500 |  |  | $4501-17200076000-1-1$ |
| 47 |  |  | 73500 | 77500 |  |  | $46-1-1725000^{46508}-1-1$ |
| 48 |  |  | 74000 | 78000 |  |  | -1-1 73800 77300-1-1 |
| 49 |  |  | 74500 | 78500 |  |  |  |
| 50 |  |  | 75500 | 79000 |  |  |  |
| 51 |  |  | 76000 | 80000 |  |  | S1-1-176000 80000-1-1 |
| 52 |  |  | 76500 |  |  |  | $52-1-176500-1-1-1$ |
| 53 |  |  | 77500 |  |  |  | $33-1-177500-1-1-1$ |
| 54 |  |  | 78000 |  |  |  | $34-1-178000-1-1-1$ |
| 55 |  |  | 78500 |  |  |  | $550-1-1785000-1-1-1$ |
| 56 |  |  | 79500 |  |  |  | 36-1-178500-1-1-1 |
| 57 |  |  | 80000 |  |  |  | 57-1-180000-1-1-1 |

Figure 4.11: Maximum truck gross weight as seen in NC §20-118 (b)(3) (left image), and as seen in statute_weights.txt (right image)

### 4.4 Output File

When the truck program is executed, an output file is produced (Trucks_out.txt). This output file displays a list of generated trucks based on the parameters set by the user in the input file. Trucks are assigned an output number, and values are listed for the following variables (all distances are feet, all loads are pounds, all moments are in pounds feet):

Axls: $\quad$ Number of axles present on generated truck

Lngth: Distance between first and last axle

NCS: Maximum gross truck weight based on NC general statute matrix

Weight: Sum of axle loads for generated truck

Ax1: $\quad$ Axle load for the first axle on generated truck $\left(A x 2=2^{\text {nd }}\right.$ axle, etc. $)$
d1: $\quad$ Distance between first and second axle for generated truck $(\mathrm{d} 2=$ distance between second and third axle, etc.)

Mmax: Maximum bending moment calculated for generated truck on the span specified in the user input file, calculated by influence line method

Span: $\quad$ Span length specified in the user input file

| Trck | Axls | Lngth | NCS | Weight | Ax1 | d1 | Ax2 | d2 | Ax 3 | Mmax | Span |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 3 | 13 | 45500 | 45500 | 15833 | 9 | 14833 | 4 | 14833 | 1036 | 100 |
| 2 | 3 | 15 | 47000 | 47000 | 16333 | 11 | 15333 | 4 | 15333 | 1054 | 100 |
| 3 | 3 | 18 | 49500 | 49500 | 17167 | 14 | 16167 | 4 | 16167 | 1085 | 100 |

## Figure 4.12: Sample output file, single vehicle, three-axles

Some constraints were placed on the potential truck configurations. As mentioned above, the shortest distance between axles (the ' $a$ ' distance) is used for all tandem axles; additionally, the ' $a$ ' distance is excluded from use as the distance between the first and second axles. For single vehicles with 3 , 4 , or 5 axles, all axle distances past axle two were considered tandem axles; for single vehicles with 6 or 7 axles, all axle distances except the first and last were considered tandem axles. For tandem trucks with three axles, no axle spacings were considered tandem axles; for tandem trucks with five axles, the last axle spacing was considered to be tandem axles. For tandem trucks with six axles, the last three axles were considered tandem axles; for tandem trucks with seven axles, axles 2 and 3 as well as axles 6 and 7 were considered tandem axles. These constraints are hard-coded into the program itself.

## Chapter 5: Results

### 5.1 Introduction

The results presented in this thesis cover two subjects. The first subject is a comparison of the legal vehicles and the North Carolina general statute governing truck weights and the exceptions delineated within. The second subject presents the results of the optimized load critical vehicle methodology, in which twenty-eight steel girder bridges were tested in NCDOTs Wearable Inspection and Grading Information Network System (WGINS). Group 1 bridges consisted of sixteen bridges tested at of percent effectiveness beginning at $100 \%$ and declining in intervals of $1 \%$ until $90 \%$ was reached, and section modulus beginning at $100 \%$ and declining in intervals of $5 \%$ until $70 \%$ was reached. Each group 1 bridge was subjected to 77 tests, for a total of 1232 tests performed on group 1 bridges. Group 2 bridges consisted of the twelve bridges tested at varying levels of percent effectiveness. Testing began at the highest level of effectiveness that resulted in no vehicles recording an operating rating factor below 1.0 and decreased in intervals of $1 \%$ until the operating rating factor for SNCOTTS3 fell below 1.0 ; the only exception was bridge \#590126, which had multiple vehicles with an operating rating factor below 1.0 at $100 \%$ efficiency. A total of 155 tests were performed on group 2 bridges. The results of these tests were compiled to determine what effect the degradation of these bridge characteristics had on the posting vehicle for the bridge.

### 5.2 Non-Compliant Legal Vehicle

A comparison of North Carolina general statute §20-118(b)(3) and the list of 16 legal vehicles utilized by NCDOT to load rate non-interstate bridges reveals that one of the legal vehicles does not comply with the general statute. SNCOTTS3 has a total length of 15 ft . and a gross weight of $54,500 \mathrm{lbs}$., as shown in Figure 5.1. According to the stature, as shown in Figure 2.2 (page 8), the maximum weight for a vehicle with three axles and a length of 15 ft . is $47,000 \mathrm{lbs}$.


Figure 5.1: SNCOTTS3 axle loads and geometry.

SNCOTTS3 represents a cotton truck, and cotton trucks have a weight exception written into the statue, as shown below in Figure 5.2. However, that exception only covers the tandem axle weight, and does not provide an exception for gross vehicle weight. According to North Carolina general statute §20-118(k):
"A vehicle which is equipped with a self-loading bed and which is designed and used exclusively to transport compressed seed cotton from the farm to a cotton gin, or sage to market, may operate on the highways of the State, except interstate highways, with a tandem-axle weight not exceeding 50,000 pounds."

To bring the legal vehicle representing cotton trucks into compliance with current law, the gross weight of the vehicle would have to be reduced to $47,000 \mathrm{lbs}$., or the vehicle length would have to be increased to 25 ft .

### 5.3 Group 1 Bridges

Group 1 bridges were found to have a consistent progression of emerging posting vehicles. In general, the operating rating factors dropped below 1.0 in a progression consistent with the vehicles' gross weights; the heaviest vehicles saw their operating rating factor drop below 1.0 first, and the rest followed in order of declining gross vehicle weight. Consequently, the heaviest vehicle in any categorization group would be the initial posting vehicle and would remain so until the next lightest vehicle's operating rating factor dropped below 1.0, at which point the lighter vehicle would become the posting vehicle.

The eight single unit legal vehicles exhibit relatively large gaps in gross vehicle weight, with one exception, as seen in Figure 3.5 (page 33). With the exception of SNAGGRIS4, each subsequent vehicle is a minimum of two tons lighter than the preceding vehicle. As a result, the progression of posting vehicles follows the declining rating vehicles, beginning with SNS7B and continuing through the cotton truck SNCOTTS3. After the cotton truck, the next two lighter two-axle vehicles have significantly higher operating weights, and the lightest vehicle, SNSH, has the lowest operating weight of all tested legal vehicles.

Figure 5.2 displays the posting single unit vehicle for all tested conditions on bridge \#220015. The progression mentioned above is visible for both methods of bridge

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 40.6 | 37.5 | 33.1 | 30.3 | 25.1 | 22.5 |
|  | 99 | \#N/A | SNS6A | SNS5A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 39.9 | 35.5 | 32.6 | 29.8 | 24.7 | 22.1 |
|  | 98 | \#N/A | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 39.3 | 34.9 | 32.1 | 26.9 | 24.3 | 21.7 |
|  | 97 | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 41.7 | 38.7 | 34.4 | 31.6 | 26.5 | 23.9 | 21.4 |
|  | 96 | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 41.1 | 38.1 | 33.9 | 31.1 | 26.0 | 23.5 | 21.0 |
|  | 95 | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 40.5 | 37.5 | 33.3 | 30.6 | 25.6 | 23.1 | 20.6 |
|  | 94 | SNS7B | SNS5A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 40.5 | 35.5 | 32.8 | 30.1 | 25.1 | 22.7 | 20.2 |
|  | 93 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 39.1 | 34.9 | 32.2 | 27.1 | 24.7 | 22.3 | 19.8 |
|  | 92 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 38.5 | 34.3 | 31.7 | 26.7 | 24.3 | 21.8 | 19.4 |
|  | 91 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 37.9 | 33.8 | 31.2 | 26.2 | 23.8 | 21.4 | 19.0 |
|  | 90 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 37.3 | 33.2 | 30.6 | 25.7 | 23.4 | 21.0 | 18.7 |

Figure 5.2: Posting single unit vehicles with operating weights for bridge \#220015.


Figure 5.3: Posting frequency of single unit vehicles for bridge \#220015.
degradation. At $100 \%$ efficiency, SNS7B emerged as the posting vehicle at $95 \%$ section modulus. At that testing condition, only SNS7B had an operating rating factor below 1.0. The operating rating factor for SNS6A fell below 1.0 at $90 \%$ section modulus; with a lower operating weight than SNS7B, SNS6A became the posting vehicle at this condition. SNS5A emerged at $85 \%$ section modulus, and SNCOTTS3 became the posting vehicle at $75 \%$. This same pattern can be seen reading Figure 5.2 vertically; at $95 \%$ section modulus, SNS7B was the posting vehicle at $100 \%$ efficiency, but SNS7B gave way to SNS6A at $99 \%$ effectiveness, and SNS5A emerged at $94 \%$ effectiveness.

Figure 5.3 shows the controlling frequency for each single unit vehicle during the tests on bridge \#220015. SNCOTTS3 was the posting vehicle for 35 of the conditions tested, SNS5A was the posting vehicle for 24 of the conditions tested, SNS6A was the posting vehicle for 10 of the conditions tested, and SNS7B was the posting vehicle for 5 of the conditions tested. As seen in Figure 5.2, there was no posting vehicle for three of the conditions tested.

The consistent pattern in group 1 for single unit vehicles is SNS7B > SNS6A > SNS5A > SNCOTTS3 > SNSH. This pattern can be seen in Figure 5.4.

Gaps or omissions in this progression present in Figure 5.5 occur for one of several reasons:

- The state of the bridge is such that, when examined at $100 \%$ effectiveness and $100 \%$ section modulus, multiple single unit vehicles already have an operating rating factor below 1.0. This occurs for bridges 490054, 100309, 310089, 010003, 310008, 240138, 220025, and 480189.

| Bridge \# | Length | Progression of controlling SU Rating Vehicle |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | First ---> |  |  |  | $--->$ Last |
| 490054 | 19.5 |  | SNS6A |  | SNCOTTS3 |  |
| 350022 | 25.0 | SNS7B | SNS6A | SNS5A | SNCOTTS3 |  |
| 100309 | 26.7 |  |  |  | SNCOTTS3 |  |
| 310089 | 30.1 |  |  |  | SNCOTTS3 | SNSH |
| 10003 | 34.3 |  |  |  | SNCOTTS3 | SNSH |
| 80037 | 36.5 | SNS7B | SNS6A | SNS5A | SNCOTTS3 |  |
| 310008 | 37.0 |  |  |  | SNCOTTS3 | SNSH |
| 110105 | 38.3 | SNS7B | SNS6A | SNS5A | SNCOTTS3 |  |
| 100152 | 39.0 | SNS7B |  |  |  |  |
| 240138 | 39.0 |  | SNS6A | SNS5A | SNCOTTS3 |  |
| 590054 | 39.5 | SNS7B | SNS6A | SNS5A | SNCOTTS3 |  |
| 330276 | 41.0 | SNS7B | SNS6A | SNS5A |  |  |
| 220025 | 44.1 |  |  | SNS5A | SNCOTTS3 |  |
| 430003 | 53.6 | SNS7B | SNS6A | SNS5A |  |  |
| 220015 | 56.4 | SNS7B | SNS6A | SNS5A | SNCOTTS3 |  |
| 480189 | 56.9 |  |  |  | SNCOTTS3 | SNSH |

Figure 5.4: Posting single unit vehicles from group 1 set, including progression.

- The state of the bridge is such that, at the lowest values tested for \% effectiveness and section modulus loss, there remain vehicles in the progression with operating rating factors above 1.0 . This happens frequently relating to vehicle SNSH, which has an operating weight well below that of SNCOTTS3. This occurs for larger vehicles for bridges 100152, 330276, and 430003 .
- Integer increments of section modulus loss or effectiveness loss obscure a vehicle that would otherwise control. This occurs for bridge 490054.

According to the data presented in Figure 5.5, at $99 \%$ effectiveness $/ 100 \%$ section modulus, both SNCOTTS3 and SNS5A had operating rating values above 1.0; at $98 \%$ effectiveness $/ 100 \%$ section modulus, both had operating rating values below 1.0. In both instances, the operating rating value for SNS5A was lower than that for SNCOTTS3; it is

|  | Vehicle Weight | Operating Weight | Inventory <br> Weight | Calculated OPER RF | Calculated INV RF |  | Vehicle Weight | Operating Weight | Inventory Weight | Calculated OPER RF | Calculated INV RF |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HS | 15.00 | 25.3 | 15.2 | 1.687 | 1.013 | HS | 15.00 | 25.0 | 15.0 | 1.667 | 1.000 |
| SNSH | 13.50 | 24.9 | 14.9 | 1.844 | 1.104 | SNSH | 13.50 | 24.6 | 14.8 | 1.822 | 1.096 |
| SNGARBS2 | 20.00 | 34.5 | 20.7 | 1.725 | 1.035 | SNGARBS2 | 20.00 | 34.1 | 20.5 | 1.705 | 1.025 |
| SNAGRIS2 | 22.00 | 40.5 | 24.3 | 1.841 | 1.105 | SNAGRIS2 | 22.00 | 40.1 | 24.0 | 1.823 | 1.091 |
| SNCOTTS3 | 27.25 | 27.4 | 16.5 | 1.006 | 0.606 | SNCOTTS3 | 27.25 | 27.1 | 16.3 | 0.994 | 0.598 |
| SNAGGRS4 | 34.92 | 35.8 | 21.5 | 1.025 | 0.616 | SNAGGRS4 | 34.92 | 35.4 | 21.2 | 1.014 | 0.607 |
| SNS5A | 35.55 | 35.6 | 21.3 | 1.001 | 0.599 | SNS5A | 35.55 | 35.2 | 21.1 | 0.990 | 0.594 |
| SNS6A | 39.95 | 38.9 | 23.3 | 0.974 | 0.583 | SNS6A | 39.95 | 38.5 | 23.1 | 0.964 | 0.578 |
| SNS7B | 42.00 | 40.9 | 24.5 | 0.974 | 0.583 | SNS7B | 42.00 | 40.4 | 24.3 | 0.962 | 0.579 |
| TNAGRIT3 | 33.00 | 51.6 | 31.0 | 1.564 | 0.939 | TNAGRIT3 | 33.00 | 51.1 | 30.6 | 1.548 | 0.927 |
| TNT4A | 33.08 | 39.0 | 23.4 | 1.179 | 0.707 | TNT4A | 33.08 | 38.6 | 23.2 | 1.167 | 0.701 |
| TNT6A | 41.60 | 44.0 | 26.4 | 1.058 | 0.635 | TNT6A | 41.60 | 43.5 | 26.1 | 1.046 | 0.627 |
| TNT7A | 42.00 | 47.3 | 28.4 | 1.126 | 0.676 | TNT7A | 42.00 | 46.8 | 28.1 | 1.114 | 0.669 |
| TNT7B | 42.00 | 42.7 | 25.6 | 1.017 | 0.610 | TNT7B | 42.00 | 42.2 | 25.3 | 1.005 | 0.602 |
| TNAGRIT4 | 43.00 | 49.0 | 29.4 | 1.140 | 0.684 | TNAGRIT4 | 43.00 | 48.4 | 29.1 | 1.126 | 0.677 |
| TNAGT5A | 45.00 | 51.2 | 30.7 | 1.138 | 0.682 | TNAGT5A | 45.00 | 50.7 | 30.4 | 1.127 | 0.676 |
| TNAGT5B | 45.00 | 51.5 | 30.9 | 1.144 | 0.687 | TNAGT5B | 45.00 | 50.9 | 30.5 | 1.131 | 0.678 |
|  | \% eff | 0.99 |  |  |  |  | \% eff | 0.98 |  |  |  |
|  | Sx $=$ | 1.0 |  |  |  |  | Sx $=$ | 1.0 |  |  |  |

Figure 5.5: Analysis results for bridge 490054 at $\mathbf{9 9 \%}$ effectiveness $/ \mathbf{1 0 0 \%}$ section modulus (left) and $\mathbf{9 8 \%}$ effectiveness $/ \mathbf{1 0 0 \%}$ section modulus (right).
therefore reasonable to conclude the operating rating factor for SNS5A would fall below 1.0 before that of SNCOTTS3, and SNS5A would control for a value of \% effectiveness between $88 \%$ and $98 \%$.

Compared to the single unit vehicles, the seven tandem trucks showed a lower degree of stratification of gross weights, as shown in Figure 3.5 (page 33). TNAGRIT3 and TNT4A are separated by 160 pounds; both five axle trucks, and both seven axle trucks, have identical gross weights; and TNT6A is only 800 pounds lighter than either of the seven axle trucks.

Figure 5.6 displays the posting tandem truck for all tested conditions on bridge \#240138. At $100 \%$ efficiency/100\% section modulus, only TNAGT5A and TNAGT5B had operating rating factors below 1.0; as TNAGT5B consistently had a lower operating weight than TNAGT5A, it was the posting vehicle at $100 \%$ efficiency/ $100 \%$ section modulus. As

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 41.3 | 38.6 | 35.9 | 31.2 | 28.7 | 26.2 | 23.7 |
|  | 99 | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 40.7 | 38.1 | 35.4 | 30.8 | 28.3 | 25.8 | 23.3 |
|  | 98 | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 40.2 | 37.6 | 32.8 | 30.4 | 27.9 | 25.4 | 22.9 |
|  | 97 | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 39.6 | 37.1 | 32.3 | 29.9 | 27.5 | 25.0 | 22.6 |
|  | 96 | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 39.1 | 36.5 | 31.9 | 29.5 | 27.1 | 24.6 | 22.2 |
|  | 95 | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 38.5 | 36.0 | 31.4 | 29.0 | 26.6 | 24.3 | 21.9 |
|  | 94 | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 38.0 | 35.5 | 31.0 | 28.6 | 26.2 | 23.9 | 21.5 |
|  | 93 | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 37.4 | 32.8 | 30.5 | 28.2 | 25.8 | 23.5 | 21.1 |
|  | 92 | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 36.9 | 32.3 | 30.0 | 27.7 | 25.4 | 23.1 | 20.8 |
|  | 91 | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 36.4 | 31.9 | 29.6 | 27.3 | 25.0 | 22.7 | 20.4 |
|  | 90 | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 35.8 | 31.4 | 29.1 | 26.8 | 24.6 | 22.3 | 20.1 |

Figure 5.6: Posting tandem trucks with operating weights for bridge \#240138.


Figure 5.7: Posting frequency of tandem trucks for bridge \#240138.
with the single unit vehicles, the progression displayed in Figure 5.6 is evident both horizontally and vertically. At $100 \%$ efficiency, TNAGT5B was the posting vehicle until $85 \%$ section modulus was tested. From that condition through all remaining declining values of section modulus, TNAGRIT3 was the posting vehicle. At $95 \%$ section modulus, TNAGT5B was the posting vehicle at $100 \%$ efficiency, and TNAGRIT3 emerged as the posting vehicle at $93 \%$ efficiency and remained the posting vehicle for all subsequent declining values of \% efficiency.

Figure 5.7 shows the controlling frequency for each tandem truck during the tests on bridge \# 240138. TNAGT5B was the posting vehicle for 20 of the conditions tested, and TNAGRIT3 was the posting vehicle for 57 of the conditions tested.

Two progression patterns are present for tandem trucks on group 1 bridges, as shown below in Figure 5.8. For spans below 31 feet, the pattern for tandem trucks is TNT7B > TNT4A; for spans above 31 feet, the pattern is TANGT5B > TNAGRIT3.

Omissions from these patterns present in Figure 5.7 occur for the following reasons:

- The state of the bridge is such that, when examined at $100 \%$ effectiveness and $100 \%$ section modulus, multiple tandem trucks already have an operating rating factor below 1.0. This occurs for bridges 310089 and 480189.
- The state of the bridge is such that, at the lowest values tested for $\%$ effectiveness and section modulus loss, there remain vehicles in the progressions with operating rating factors above 1.0. This occurs for bridges 330276 and 430003. This also
occurs for bridge 100152, for which none of the tandem trucks recorded an operating rating factor below 1.0.

| Bridge \# | Length | Progression of controlling TT Rating Vehicle |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | First ---> |  |  | $--->$ Last |
| 490054 | 19.5 |  | TNT7B | TNT4A |  |
| 350022 | 25.0 |  | TNT7B | TNT4A |  |
| 100309 | 26.7 |  | TNT7B | TNT4A |  |
| 310089 | 30.1 |  |  | TNT4A |  |
| 10003 | 34.3 |  |  |  | TNAGRIT3 |
| 80037 | 36.5 | TNAGT5B |  |  | TNAGRIT3 |
| 310008 | 37.0 |  |  |  | TNAGRIT3 |
| 110105 | 38.3 | TNAGT5B |  |  | TNAGRIT3 |
| 100152 | 39.0 |  |  |  |  |
| 240138 | 39.0 | TNAGT5B |  |  | TNAGRIT3 |
| 590054 | 39.5 | TNAGT5B |  |  | TNAGRIT3 |
| 330276 | 41.0 | TNAGT5B |  |  |  |
| 220025 | 44.1 | TNAGT5B |  |  | TNAGRIT3 |
| 430003 | 53.6 | TNAGT5B |  |  |  |
| 220015 | 56.4 | TNAGT5B |  |  | TNAGRIT3 |
| 480189 | 56.9 |  |  |  | TNAGRIT3 |

Figure 5.8: Posting tandem trucks from group 1 set, including progression.

### 5.4 Group 2 Bridges

Group 2 bridges generally followed then same progression pattern as the group 1 bridges, with some minor differences and inclusions. Single unit vehicles continue to follow the pattern SNS7A > SNS6A > SNS5A > SNCOTTS3, although SNAGGRS4 does appear as a posting vehicle on three of the bridges (Figure 5.9). As seen in the group 1 bridges, there is an instance where the bridge condition is such that multiple vehicles have

| Bridge \# | Length | Progression of controlling SV Rating Vehicle |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | First ---> |  |  |  | ---> Last |
| 330305 | 50.8 | SNS7B | SNS6A | SNS5A |  | SNCOTTS3 |
| 330049 | 55.3 | SNS7B | SNS6A | SNS5A |  | SNCOTTS3 |
| 330048 | 63.8 | SNS7B | SNS6A | SNS5A |  | SNCOTTS3 |
| 330302 | 69.6 | SNS7B | SNS6A | SNS5A |  | SNCOTTS3 |
| 500062 | 71.2 | SNS7B | SNS6A | SNS5A |  | SNCOTTS3 |
| 840010 | 74.9 | SNS7B | SNS6A | SNS5A | SNAGGRS4 | SNCOTTS3 |
| 590404 | 91.9 | SNS7B | SNS6A | SNS5A |  | SNCOTTS3 |
| 590169 | 97.7 | SNS7B | SNS6A | SNS5A |  | SNCOTTS3 |
| 590126 | 111.6 |  |  | SNS5A | SNAGGRS4 | SNCOTTS3 |
| 90096 | 119.3 | SNS7B | SNS6A | SNS5A |  | SNCOTTS3 |
| 590516 | 121.1 | SNS7B | SNS6A | SNS5A |  | SNCOTTS3 |
| 590182 | 162.9 |  | SNS6A |  | SNAGGRS4 | SNCOTTS3 |

Figure 5.9: Posting single unit vehicles from group 2 set, including progression.
an operating rating factor below 1.0 at the maximum values for $\%$ effectiveness and section modulus; this occurs for bridge 590126. There is also a bridge where a gap in the progression occurs when multiple vehicles have an operating rating factor fall below 1.0 at the same time; this occurs for bridge 590182 as the $\%$ effectiveness falls from $58 \%$ to $57 \%$. As seen previously, if the change in effectiveness occurs below the level of whole integers, SNS7B would control at a point between $58 \%$ and $57 \%$ effectiveness.

Progression for the group 2 tandem trucks follows the pattern evident in the longer group 1 bridges, TNAGT5B > TNAGRIT3, although again a few other vehicles appeared in the intermediate range (Figure 5.10). Of interest is the reemergence of TNT4A as a posting vehicle over TNAGRIT3 on two of the longer spans, something previously seen in spans shorter than 30.1 feet; this occurs for bridge 590169 and 590182, where the operating weight for TNT4A is consistently lower than the operating weight for TNAGRIT3. Additional posting tandem trucks present in group 2 include TNT6A and TNAGRIT4.

| Bridge \# | Length | Progression of controlling TT Rating Vehicle |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | First ---> |  |  |  | ---> Last |
| 330305 | 50.8 | TNAGT5B |  |  |  | TNAGRIT3 |
| 330049 | 55.3 | TNAGT5B |  |  |  | TNAGRIT3 |
| 330048 | 63.8 | TNAGT5B |  |  |  | TNAGRIT3 |
| 330302 | 69.6 | TNAGT5B |  |  |  | TNAGRIT3 |
| 500062 | 71.2 | TNAGT5B |  |  |  | TNAGRIT3 |
| 840010 | 74.9 | TNAGT5B |  |  |  | TNAGRIT3 |
| 590404 | 91.9 | TNAGT5B |  |  |  | TNAGRIT3 |
| 590169 | 97.7 | TNAGT5B |  |  |  |  |
| 590126 | 111.6 | TNAGT5B |  |  |  | TNT4A |
| 90096 | 119.3 | TNAGT5B |  | TNT6A |  | TNAGRIT3 |
| 590516 | 121.1 | TNAGT5B |  | TNT6A |  | TNAGRIT3 |
| 590182 | 162.9 | TNAGT5B | TNAGRIT4 |  | TNT4A |  |

Figure 5.10: Posting tandem trucks from group 2 set, including progression.

The additional posting trucks present in the group 2 analysis can all be considered redundant. Three group 2 bridges have an additional posting single unit vehicle, SNAGGRIS4. This vehicle controls whenever it has an operating weight equal to or less than that of SNS5A. For the three bridges where SNAGGRIS4 appears in the posting progression, the difference in operating weight between it and SNS5A is never more than 200 lbs., as seen in Figure 5.11 below:

| 840010 |  |  |
| :---: | :---: | :---: |
| $\%$ <br> Eff | Vehicle | OP <br> Weight <br> $(\mathrm{k} * \mathrm{ft})$ |
| 55 | SNAGGRS4 | 31.5 |
|  | SNS5A | 31.4 |
|  |  |  |
| 54 | SNAGGRS4 | 30.9 |
|  | SNS5A | 30.9 |
| 53 | SNAGGRS4 | 30.4 |
|  | SNS5A | 30.3 |


| 590126 |  |  |
| :---: | :---: | :---: |
| $\%$ <br> Eff | Vehicle | OP <br> Weight <br> $(\mathrm{k} * \mathrm{ft})$ |
| 98 | SNAGGRS4 | 33.2 |
|  | SNS5A | 33.1 |
| 97 | SNAGGRS4 | 32.4 |
|  | SNS5A | 32.4 |
| 96 | SNAGGRS4 | 31.7 |
|  | SNS5A | 31.6 |


| 590182 |  |  |
| :---: | :---: | :---: |
| $\%$ <br> Eff | Vehicle | OP <br> Weight <br> $(\mathrm{k} * \mathrm{ft})$ |
| 55 | SNAGGRS4 | 33.9 |
|  | SNS5A | 33.9 |
|  |  |  |
| 54 | SNAGGRS4 | 31.3 |
|  | SNS5A | 31.4 |
|  |  |  |
| 53 | SNAGGRS4 | 28.8 |
|  | SNS5A | 28.8 |

Figure 5.11: Operating weight comparison for group 2 single unit vehicles.

In all three instances where SNAGGRS4 appears in Figure 5.11, it only temporarily controls over SNS5A when the weight difference between the two vehicles is less than 100 lbs., and the total operating weight difference between the two in all testing conditions never rises above 200 lbs.

Three group 2 bridges have one of two additional posting tandem trucks, TNT6A and TNAGRIT4 (Figure 5.10). As seen before with the single unit vehicles, these two additional vehicles only control when they have an operating weight within 200 lbs . of another vehicle that typically controls, as shown in Figure 5.12 below:

| 90096 |  |  | 590516 |  |  | 590182 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \% \\ & \text { Eff } \end{aligned}$ | Vehicle | OP Weight ( $\mathrm{k} * \mathrm{ft}$ ) | $\begin{aligned} & \% \\ & \text { Eff } \end{aligned}$ | Vehicle | OP Weight ( $\mathrm{k} * \mathrm{ft}$ ) | \% | Vehicle | $\begin{gathered} \hline \text { OP } \\ \text { Weight } \\ (\mathrm{k} * \mathrm{ft}) \end{gathered}$ |
| 55 | TNT6A TNAGT5B | $\begin{aligned} & 38.8 \\ & 38.7 \end{aligned}$ | 53 | TNT6A TNAGT5B | $\begin{aligned} & \hline 42.7 \\ & 42.6 \end{aligned}$ | 57 | TNAGRIT4 TNAGT5B | $\begin{aligned} & 40.1 \\ & 40.0 \end{aligned}$ |
| 54 | TNT6A TNAGT5B | $\begin{aligned} & 37.0 \\ & 37.0 \end{aligned}$ | 52 | TNT6A TNAGT5B | $\begin{aligned} & 40.6 \\ & 40.6 \end{aligned}$ | 56 | TNAGRIT4 TNAGT5B | $\begin{aligned} & 37.4 \\ & 37.4 \end{aligned}$ |
| 53 | $\begin{gathered} \text { TNT6A } \\ \text { TNAGT5B } \end{gathered}$ | $\begin{aligned} & 35.3 \\ & 35.3 \end{aligned}$ | 51 | $\begin{gathered} \text { TNT6A } \\ \text { TNAGT5B } \end{gathered}$ | $\begin{aligned} & 38.6 \\ & 38.5 \end{aligned}$ | 55 | TNAGRIT4 <br> TNAGT5B | $\begin{aligned} & 34.8 \\ & 347 \end{aligned}$ |
| 52 | $\begin{gathered} \text { TNT6A } \\ \text { TNAGT5B } \\ \hline \end{gathered}$ | $\begin{array}{r} 33.6 \\ 33.5 \\ \hline \end{array}$ | 50 | $\begin{gathered} \text { TNT6A } \\ \text { TNAGT5B } \end{gathered}$ | $\begin{aligned} & 36.5 \\ & 36.5 \end{aligned}$ |  |  |  |
|  |  |  | 49 | $\begin{gathered} \text { TNT6A } \\ \text { TNAGT5B } \end{gathered}$ | $\begin{aligned} & 34.4 \\ & 34.4 \end{aligned}$ |  |  |  |
|  |  |  | 48 | $\begin{gathered} \text { TNT6A } \\ \text { TNAGT5B } \\ \hline \end{gathered}$ | $\begin{aligned} & 32.4 \\ & 32.3 \end{aligned}$ |  |  |  |

## Figure 5.12: Operating weight comparison for group 2 tandem trucks.

TNT6A appears in the progression of posting vehicles on two bridges, and only in instances where the operating weight of that vehicle is within 200 lbs . of an established posting vehicle, TNAGT5B. For bridge 590516, TNT6A appears twice, in non-contiguous

| Group 1 Totals |  | Group 2 Totals |  | All Bridge Totals |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| All Vehicles |  | All Vehicles |  | All Vehicles |  |
| Vehicle | Count | Vehicle | Count | Vehicle | Count |
| HS | 0 | HS | 0 | HS | 0 |
| SNSH | 53 | SNSH | 0 | SNSH | 0 |
| SNGARBS2 | 0 | SNGARBS2 | 0 | SNGARBS2 | 0 |
| SNAGRIS2 | 0 | SNAGRIS2 | 0 | SNAGRIS2 | 0 |
| SNCOTTS3 | 672 | SNCOTTS3 | 21 | SNCOTTS3 | 92 |
| SNAGGRS4 | 0 | SNAGGRS4 | 5 | SNAGGRS4 | 5 |
| SNS5A | 122 | SNS5A | 64 | SNS5A | 82 |
| SNS6A | 54 | SNS6A | 27 | SNS6A | 39 |
| SNS7B | 40 | SNS7B | 18 | SNS7B | 23 |
| TNAGRIT3 | 0 | TNAGRIT3 | 0 | TNAGRIT3 | 0 |
| TNT4A | 0 | TNT4A | 0 | TNT4A | 0 |
| TNT6A | 0 | TNT6A | 0 | TNT6A | 0 |
| TNT7A | 0 | TNT7A | 0 | TNT7A | 0 |
| TNT7B | 0 | TNT7B | 0 | TNT7B | 0 |
| TNAGRIT4 | 0 | TNAGRIT4 | 0 | TNAGRIT4 | 0 |
| TNAGT5A | 0 | TNAGT5A | 0 | TNAGT5A | 0 |
| TNAGT5B | 4 | TNAGT5B | 10 | TNAGT5B | 11 |
| Single Unit |  | Single Unit |  | Single Unit |  |
| Vehicle | Count | Vehicle | Count | Vehicle | Count |
| HS | 0 | HS | 0 | HS | 0 |
| SNSH | 53 | SNSH | 0 | SNSH | 0 |
| SNGARBS2 | 0 | SNGARBS2 | 0 | SNGARBS2 | 0 |
| SNAGRIS2 | 0 | SNAGRIS2 | 0 | SNAGRIS2 | 0 |
| SNCOTTS3 | 672 | SNCOTTS3 | 21 | SNCOTTS3 | 92 |
| SNAGGRS4 | 0 | SNAGGRS4 | 5 | SNAGGRS4 | 5 |
| SNS5A | 122 | SNS5A | 64 | SNS5A | 84 |
| SNS6A | 54 | SNS6A | 27 | SNS6A | 37 |
| SNS7B | 40 | SNS7B | 18 | SNS7B | 23 |
| Tandem Trucks |  | Tandem Trucks |  | Tandem Trucks |  |
| Vehicle | Count | Vehicle | Count | Vehicle | Count |
| TNAGRIT3 | 428 | TNAGRIT3 | 42 | TNAGRIT3 | 80 |
| TNT4A | 246 | TNT4A | 8 | TNT4A | 29 |
| TNT6A | 0 | TNT6A | 6 | TNT6A | 6 |
| TNT7A | 0 | TNT7A | 0 | TNT7A | 0 |
| TNT7B | 48 | TNT7B | 0 | TNT7B | 12 |
| TNAGRIT4 | 0 | TNAGRIT4 | 1 | TNAGRIT4 | 1 |
| TNAGT5A | 0 | TNAGT5A | 0 | TNAGT5A | 0 |
| TNAGT5B | 206 | TNAGT5B | 87 | TNAGT5B | 113 |

Figure 5.13: Total occurrences for posting vehicles across all bridge tests.
levels of \% effectiveness, and only controls when that vehicle has an operating weight within 100 lbs . of TNAGT5B. TNAGRIT4 only appears in the posting progression once, on one bridge, and that occurs when hat vehicle has an operating weight within 100 lbs . of TNAGT5B.

### 5.5 Posting Vehicle Frequency

In Figure 5.12, the total counts for posting vehicles across all bridge tests conducted in WIGINS is displayed; the total counts for single unit vehicles is displayed in Figure 5.13, and the total counts for tandem trucks us displayed in Figure 5.14. Group 1 totals reflect tests executed on group 1 bridges for all declining values of $\%$ effectiveness and section modulus loss; for the 16 bridges analyzed, this returned a total of 1232 possible


Figure 5.14: Posting vehicle frequency for all group 1 vehicles.
posting vehicles. None of the individual groups (all vehicles, single unit vehicles, tandem trucks) combine to 1232 vehicles due to the instances where there were no vehicles with an operating rating value below 1.0 at that specific instance. Results were grouped in three ways: first, all vehicles; then single unit vehicles only; and lastly, tandem trucks only.


Figure 5.15: Posting vehicle frequency for all group 1 single unit vehicles.


Figure 5.16: Posting vehicle frequency for all group 1 tandem trucks.

Group 2 totals shown in Figure 5.17 reflect tests executed on group 2 bridges at full section modulus and declining values of $\%$ effectiveness. Results were grouped in three ways: first, all vehicles; then single unit vehicles only; and lastly, tandem trucks only.


Figure 5.17: Posting vehicle frequency for all group 2 vehicles.


Figure 5.18: Posting vehicle frequency for all group 2 single unit vehicles.


Figure 5.19: Posting vehicle frequency for all group 2 tandem trucks.

All bridge totals, as shown in Figure 5.20, were a result of combining the results from the group 2 analysis shown above with results taken from group 1 analysis; for the purpose of this analysis, only results from group 1 bridges at $100 \%$ section modulus were


Figure 5.20: Posting vehicle frequency for all vehicles at $\mathbf{1 0 0 \%}$ section modulus.
considered. In Figure 5.21, the total vehicle counts for single unit vehicles is displayed, and the total vehicle counts for tandem trucks is displayed in Figure 5.22.


Figure 5.21: Posting vehicle frequency for all single unit vehicles at $\mathbf{1 0 0 \%}$ section modulus.


Figure 5.22: Posting vehicle frequency for all tandem trucks at $100 \%$ section modulus.

In Figure 5.21, the data illustrates how four single unit vehicles represented the majority of posting vehicles during the conducted tests. Two hundred forty-one single unit vehicles were found to be the posting vehicle during the $100 \%$ efficiency testing; SNAGGRS4 was calculated to be the posting vehicle 5 times.

In Figure 5.22, the data illustrates how three tandem trucks represented the majority of posting vehicles during the conducted tests. 241 tandem trucks were found to be the posting vehicle during the $100 \%$ efficiency testing; TNAGRIT4 occurs as the posting vehicle once, and TNT6A occurs as the posting vehicle 6 times.

### 5.6 Summary

Testing of steel girder bridges at progressive levels of \% efficiency and section modulus loss revealed common progressions of posting vehicles. For single unit vehicles, SNS7B was consistently the first vehicle with an operating rating factor to fall below 1.0 ; that vehicle would be the posting vehicle until the rating factor for SNS6A fell below 1.0. The progression for single unit vehicles was found to be SNS7B > SNS6A > SNS5A > SNCOTTS3 > SNSH. SNAGGRS4 occurred as a posting vehicle five times; in all such instances, the operating weight for SNAGGRS4 was within 100 lbs . of SNS5A.

For tandem trucks, two progressions were found: TNAGT5B > TNAGRIT3 and TNT7B > TNT4A. TNT6A occurred as the posting vehicle six times, and TNAGRIT4 occurred as the posting vehicle once; in all such instances, the operating weights for TNT6A or TNAGRIT4 was within 100 lbs . of TNAGT5B.

Finally, there were four vehicles that were never identified by the analysis as a posting vehicle in these tests: SNGARBS2, SNAGRIS2, TNT7A, and TNAGT5A.

## Chapter 6: Conclusions and Recommendations

### 6.1 Conclusions

NCDOT is currently responsible for managing 13,558 bridges, over 4000 of which are weight restricted, and this number is increasing as the statewide network is expanded and improved. These bridges are required to be inspected every two years. The NCDOT currently load rates bridges for thirteen vehicles that can legally travel on interstate highways and sixteen vehicles that can legally travel on non-interstate highways. The NC general statutes provides allowable axle loads at varying spacing. The process of determining the controlling load rating (or vehicle) is cumbersome, especially on multispan bridges. Maintenance of the fleet of vehicles required to perform these load ratings on the bridges managed by the NCDOT is unnecessarily burdensome. Many states have optimized their respective legal loads to a more manageable number of rating and posting vehicles, in an effort to streamline the live load generation process.

This study had three objectives, as presented in Section 1.1:

1. Develop a methodology to optimize existing NC posting vehicles.
2. Utilize the developed framework to optimize the list of posting vehicles.
3. Develop an automated computer model that generates NC posting vehicles from NC general statutes.

The developed methodology determined the posting vehicle for 28 steel girder bridges; the sixteen bridges comprising group 1 were tested for all 16 non-interstate trucks at varying levels of bridge effectiveness and varying levels of section modulus loss, and the twelve bridges comprising group two were tested for all 16 non-interstate trucks at varying levels of bridge effectiveness.

This methodology was then utilized to optimize the list of posting vehicles. This process showed a distinct and consistent progression of vehicles' rating factors falling below 1.0. The observed progressions included a total of twelve of the sixteen legal vehicles. Three of these vehicles were found to be redundant for load rating purposes. As a result, the optimized list of legal vehicles used to load rate steel girder bridges may be reduced to the vehicles that appear in the controlling progression.

Based on the analysis performed, as described in Chapters 3 and 5, the following vehicles should be included in the optimized list:

- SNSH. This legal vehicle is a representation of a school bus. An example of such a vehicle is the Thomas Minotour.
- SNCOTTS3. This legal vehicle is a representation of a cotton truck. An example of such a vehicle is the Kenworth T800 cotton truck.
- SHS5A. This legal vehicle is a representation of a truck chassis used in garbage trucks, dump trucks, and concrete mixers. An example of such a vehicle is the McNeilus 5-axle front loading garbage truck.
- SNS6A. This legal vehicle is a representation of a truck chassis used in garbage trucks, dump trucks, and concrete mixers. An example of such a vehicle is the Freightliner 114SD 6-axle dump truck.
- SNS7B. This legal vehicle is a representation of a truck chassis used in garbage trucks, dump trucks, and concrete mixers. An example of such a vehicle is the Terex FDB7000 concrete mixer.
- TNAGRIT3. This legal vehicle is a representation of a two-axle tractor and a one-axle trailer. An example of such a vehicle is an International 86004 x 2 tractor hauling a 22 ft . Jet steel grain trailer
- TNT4A. This legal vehicle is a representation of a two-axle tractor and a two-axle trailer. An example of such a vehicle is an International $86004 \times 2$ tractor hauling a 40 ft . Great Dane Champion semi-trailer.
- TNAGT5B. This legal vehicle is a representation of a three-axle tractor and a two-axle trailer. An example of such a vehicle is a Peterbilt 579 tractor hauling a 40 ft . Great Dane Champion semitrailer.
- TNT7B. This legal vehicle is a notional vehicle, designed without a specific counterpart in use in the trucking industry.

SNCOTTS3 should be re-evaluated, due to non-compliance with NC general statute §20-118. Recommendations for a legally compliant legal cotton vehicle include a
version with the current axle geometry and a reduced gross weight of $47,000 \mathrm{lbs}$., or a vehicle with the current axle loads and a truck length of 25 ft .

A computer program was developed to generate potential vehicles that comply with the NC general statutes (including exceptions) that could be used in the load rating process. This program consists of input files and an executable program. The input files contain the NC Statute Matrix and the user-defined input variables; the executable program utilizes the input files to produce an output file consisting of a list of generated trucks based on the parameters set by the user in the input file. The output file is organized by truck type and number of axles and is sorted in declining values of maximum bending moment.

### 6.2 Limitations

This study tested the impact of non-interstate vehicles on steel girder bridges at declining levels of effectiveness and section modulus loss. As such, legal vehicles used on interstate bridges were not considered past the maximum bending moment calculations, and the impact of legal vehicles on other bridge types fell outside of the scope of study.

### 6.3 Recommendations

The results of this study can be used as the foundation of future research into the impact of legal vehicles on other bridge types, including box beam, concrete beam, and truss bridges. Additionally, the methodology presented in this study could be used to execute a similar study on the effect of legal vehicles on interstate bridges. Research
comparing the list of legal vehicles used for non-interstate bridges with the list of legal vehicles used on interstate bridges, in an attempt to determine vehicle redundancy between the two lists, could prove to be of considerable value. An updated legal version of the cotton truck, one in compliance with NC general statute §20-118, will need to be the subject of further testing to determine whether it will remain in the optimized list of posting vehicles. Further research may explore whether HL-93 would be sufficient for all bridge load rating, as is currently done in 17 states. This study represents the first critical step in the lengthy and ongoing process of optimizing the list of legal vehicles used by NCDOT to load rate bridges.

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Appendix I:

## WIGINS Bridge Analysis Data

Group 1 Bridges, Rating Vehicles:

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 22.1 | 20.5 | 18.8 | 17.2 | 15.6 | 13.9 | 12.1 |
|  | 99 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 21.8 | 20.2 | 18.5 | 16.9 | 15.3 | 13.7 | 11.9 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 21.5 | 19.9 | 18.2 | 16.6 | 15.0 | 13.2 | 11.7 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 21.1 | 19.5 | 17.9 | 16.3 | 14.8 | 13.0 | 11.4 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 20.8 | 19.2 | 17.6 | 16.0 | 14.5 | 12.7 | 11.2 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 20.5 | 18.9 | 17.3 | 15.8 | 14.2 | 12.5 | 11.0 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 20.1 | 18.6 | 17.0 | 15.5 | 13.9 | 12.2 | 10.7 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 19.8 | 18.3 | 16.7 | 15.2 | 13.7 | 12.0 | 10.5 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH | SNSH |
|  |  | 19.4 | 17.9 | 16.4 | 14.9 | 13.2 | 11.8 | 10.3 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH | SNSH |
|  |  | 19.1 | 17.6 | 16.1 | 14.6 | 13.0 | 11.5 | 10.0 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH | SNSH |
|  |  | 18.8 | 17.3 | 15.8 | 14.3 | 12.7 | 11.3 | 9.8 |



Bridge 010003, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 22.1 | 20.5 | 18.8 | 17.2 | 15.6 | 13.9 | 12.1 |
|  | 99 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 21.8 | 20.2 | 18.5 | 16.9 | 15.3 | 13.7 | 11.9 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 21.5 | 19.9 | 18.2 | 16.6 | 15.0 | 13.2 | 11.7 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 21.1 | 19.5 | 17.9 | 16.3 | 14.8 | 13.0 | 11.4 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 20.8 | 19.2 | 17.6 | 16.0 | 14.5 | 12.7 | 11.2 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 20.5 | 18.9 | 17.3 | 15.8 | 14.2 | 12.5 | 11.0 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 20.1 | 18.6 | 17.0 | 15.5 | 13.9 | 12.2 | 10.7 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 19.8 | 18.3 | 16.7 | 15.2 | 13.7 | 12.0 | 10.5 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH | SNSH |
|  |  | 19.4 | 17.9 | 16.4 | 14.9 | 13.2 | 11.8 | 10.3 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH | SNSH |
|  |  | 19.1 | 17.6 | 16.1 | 14.6 | 13.0 | 11.5 | 10.0 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH | SNSH |
|  |  | 18.8 | 17.3 | 15.8 | 14.3 | 12.7 | 11.3 | 9.8 |



Bridge 010003, Single Unit Vehicles


Bridge 010003, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 38.8 | 33.0 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.9 | 38.3 | 32.5 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.3 | 35.2 | 32.1 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.8 | 34.7 | 31.6 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | N/A | 40.2 | 34.2 | 27.0 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | N/A | 39.4 | 33.8 | 26.6 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | N/A | 38.9 | 33.3 | 26.2 |
|  | 93 | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 41.7 | 38.3 | 32.8 | 25.8 |
|  | 92 | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 41.1 | 35.2 | 32.3 | 25.4 |
|  | 91 | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 40.5 | 34.7 | 31.8 | 25.0 |
|  | 90 | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 39.7 | 34.2 | 27.1 | 24.6 |



Bridge 080037, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 38.8 | 33.0 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.9 | 38.3 | 32.5 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.3 | 35.2 | 32.1 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.8 | 34.7 | 31.6 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | N/A | 40.2 | 34.2 | 27.0 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | N/A | 39.4 | 33.8 | 26.6 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | N/A | 38.9 | 33.3 | 26.2 |
|  | 93 | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 41.7 | 38.3 | 32.8 | 25.8 |
|  | 92 | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 41.1 | 35.2 | 32.3 | 25.4 |
|  | 91 | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 40.5 | 34.7 | 31.8 | 25.0 |
|  | 90 | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 39.7 | 34.2 | 27.1 | 24.6 |

RV Controlling Frequency, Single Unit Vehicles


Bridge 080037, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 42.5 | 38.7 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 41.9 | 38.2 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 41.3 | 37.7 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 44.4 | 40.8 | 37.2 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 43.7 | 40.2 | 36.6 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 43.1 | 39.6 | 36.1 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 42.5 | 39.1 | 35.6 |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGRIT3 |
|  |  | N/A | N/A | N/A | N/A | 41.9 | 38.5 | 32.7 |
|  | 92 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 |
|  |  | N/A | N/A | N/A | 44.7 | 41.3 | 37.9 | 32.2 |
|  | 91 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 |
|  |  | N/A | N/A | N/A | 44.1 | 40.7 | 37.4 | 31.7 |
|  | 90 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 |
|  |  | N/A | N/A | N/A | 43.4 | 40.1 | 36.8 | 31.2 |



Bridge 080037, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 91 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 90 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | 41.9 |

RV Controlling Frequency, All Vehicles


Bridge 100152, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 91 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 90 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | 41.9 |

RV Controlling Frequency, Single Unit Vehicles


Bridge 100152, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 91 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
|  | 90 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | N/A |



Bridge 100152, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.1 | 23.7 | 22.4 | 21.0 | 19.6 | 18.2 | 16.8 |
|  | 99 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 24.8 | 23.5 | 22.1 | 20.7 | 19.3 | 18.0 | 16.6 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 24.5 | 23.2 | 21.8 | 20.5 | 19.1 | 17.8 | 16.4 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 24.2 | 22.9 | 21.6 | 20.3 | 18.9 | 17.6 | 16.2 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 24.0 | 22.7 | 21.3 | 20.0 | 18.7 | 17.3 | 16.0 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 23.7 | 22.4 | 21.1 | 19.8 | 18.4 | 17.1 | 15.8 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 23.4 | 22.1 | 20.8 | 19.5 | 18.2 | 16.9 | 15.6 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 23.1 | 21.8 | 20.6 | 19.3 | 18.0 | 16.7 | 15.4 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.8 | 21.6 | 20.3 | 19.1 | 17.8 | 16.5 | 15.2 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.6 | 21.3 | 20.1 | 18.8 | 17.5 | 16.3 | 15.0 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.3 | 21.0 | 19.8 | 18.6 | 17.3 | 16.1 | 14.8 |



Bridge 100309, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.1 | 23.7 | 22.4 | 21.0 | 19.6 | 18.2 | 16.8 |
|  | 99 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 24.8 | 23.5 | 22.1 | 20.7 | 19.3 | 18.0 | 16.6 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 24.5 | 23.2 | 21.8 | 20.5 | 19.1 | 17.8 | 16.4 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 24.2 | 22.9 | 21.6 | 20.3 | 18.9 | 17.6 | 16.2 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 24.0 | 22.7 | 21.3 | 20.0 | 18.7 | 17.3 | 16.0 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 23.7 | 22.4 | 21.1 | 19.8 | 18.4 | 17.1 | 15.8 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 23.4 | 22.1 | 20.8 | 19.5 | 18.2 | 16.9 | 15.6 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 23.1 | 21.8 | 20.6 | 19.3 | 18.0 | 16.7 | 15.4 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.8 | 21.6 | 20.3 | 19.1 | 17.8 | 16.5 | 15.2 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.6 | 21.3 | 20.1 | 18.8 | 17.5 | 16.3 | 15.0 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.3 | 21.0 | 19.8 | 18.6 | 17.3 | 16.1 | 14.8 |



Bridge 100309, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 37.3 | 31.5 | 29.7 | 27.8 | 26.0 | 24.1 | 22.3 |
|  | 99 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 32.9 | 31.1 | 29.3 | 27.5 | 25.7 | 23.9 | 22.0 |
|  | 98 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 32.6 | 30.8 | 29.0 | 27.2 | 25.4 | 23.6 | 21.7 |
|  | 97 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 32.2 | 30.4 | 28.7 | 26.9 | 25.1 | 23.3 | 21.5 |
|  | 96 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 31.8 | 30.1 | 28.3 | 26.6 | 24.8 | 23.0 | 21.2 |
|  | 95 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 31.4 | 29.7 | 28.0 | 26.2 | 24.5 | 22.7 | 21.0 |
|  | 94 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 31.1 | 29.4 | 27.6 | 25.9 | 24.2 | 22.4 | 20.7 |
|  | 93 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 30.7 | 29.0 | 27.3 | 25.6 | 23.9 | 22.2 | 20.4 |
|  | 92 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 30.3 | 28.6 | 27.0 | 25.3 | 23.6 | 21.9 | 20.2 |
|  | 91 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 29.9 | 28.3 | 26.6 | 25.0 | 23.3 | 21.6 | 19.9 |
|  | 90 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 29.6 | 27.9 | 26.3 | 24.6 | 23.0 | 21.3 | 19.6 |



Bridge 100309, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 40.4 | 34.5 | 31.3 | 24.5 |
|  | 99 | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 39.6 | 34.0 | 26.9 | 24.1 |
|  | 98 | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 39.1 | 33.4 | 26.4 | 23.7 |
|  | 97 | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 38.5 | 32.9 | 26.0 | 23.3 |
|  | 96 | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | 41.4 | 35.4 | 32.4 | 25.6 | 22.9 |
|  | 95 | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | 40.8 | 34.9 | 31.9 | 25.1 | 22.5 |
|  | 94 | \#N/A | \#N/A | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | 39.9 | 34.3 | 31.4 | 24.7 | 22.1 |
|  | 93 | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | 39.3 | 33.8 | 26.9 | 24.3 | 21.7 |
|  | 92 | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | 38.7 | 33.2 | 26.4 | 23.9 | 21.3 |
|  | 91 | \#N/A | SNS7B | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 41.4 | 38.0 | 32.6 | 26.0 | 23.4 | 20.9 |
|  | 90 | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 40.7 | 35.0 | 32.1 | 25.5 | 23.0 | 20.5 |

RV Controlling Frequency, All Vehicles


Bridge 110105, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 40.4 | 34.5 | 31.3 | 24.5 |
|  | 99 | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 39.6 | 34.0 | 26.9 | 24.1 |
|  | 98 | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 39.1 | 33.4 | 26.4 | 23.7 |
|  | 97 | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 38.5 | 32.9 | 26.0 | 23.3 |
|  | 96 | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | 41.4 | 35.4 | 32.4 | 25.6 | 22.9 |
|  | 95 | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | 40.8 | 34.9 | 31.9 | 25.1 | 22.5 |
|  | 94 | \#N/A | \#N/A | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | 39.9 | 34.3 | 31.4 | 24.7 | 22.1 |
|  | 93 | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | 39.3 | 33.8 | 26.9 | 24.3 | 21.7 |
|  | 92 | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | N/A | 38.7 | 33.2 | 26.4 | 23.9 | 21.3 |
|  | 91 | \#N/A | SNS7B | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 41.4 | 38.0 | 32.6 | 26.0 | 23.4 | 20.9 |
|  | 90 | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 40.7 | 35.0 | 32.1 | 25.5 | 23.0 | 20.5 |

RV Controlling Frequency, Single Unit Vehicles


Bridge 110105, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 |
|  |  | N/A | N/A | N/A | 43.8 | 40.1 | 36.4 | 30.5 |
|  | 99 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 |
|  |  | N/A | N/A | N/A | 43.2 | 39.5 | 35.8 | 30.0 |
|  | 98 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 |
|  |  | N/A | N/A | N/A | 42.5 | 38.9 | 35.3 | 29.5 |
|  | 97 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 |
|  |  | N/A | N/A | N/A | 41.9 | 38.3 | 32.5 | 29.0 |
|  | 96 | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 |
|  |  | N/A | N/A | 44.8 | 41.2 | 37.7 | 31.9 | 28.5 |
|  | 95 | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 |
|  |  | N/A | N/A | 44.1 | 40.6 | 37.1 | 31.4 | 28.0 |
|  | 94 | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 |
|  |  | N/A | N/A | 43.4 | 39.9 | 36.5 | 30.8 | 27.5 |
|  | 93 | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 |
|  |  | N/A | N/A | 42.8 | 39.3 | 35.9 | 30.3 | 27.0 |
|  | 92 | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 |
|  |  | N/A | N/A | 42.1 | 38.6 | 35.3 | 29.8 | 26.5 |
|  | 91 | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | N/A | 44.8 | 41.4 | 38.0 | 32.4 | 29.2 | 26.0 |
|  | 90 | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | N/A | 44.1 | 40.7 | 37.3 | 31.9 | 28.7 | 25.5 |



Bridge 110105, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 40.6 | 37.5 | 33.1 | 30.3 | 25.1 | 22.5 |
|  | 99 | \#N/A | SNS6A | SNS5A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 39.9 | 35.5 | 32.6 | 29.8 | 24.7 | 22.1 |
|  | 98 | TNAGT5B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 44.4 | 39.3 | 34.9 | 32.1 | 26.9 | 24.3 | 21.7 |
|  | 97 | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 41.7 | 38.7 | 34.4 | 31.6 | 26.5 | 23.9 | 21.4 |
|  | 96 | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 41.1 | 38.1 | 33.9 | 31.1 | 26.0 | 23.5 | 21.0 |
|  | 95 | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 40.5 | 37.5 | 33.3 | 30.6 | 25.6 | 23.1 | 20.6 |
|  | 94 | SNS7B | SNS5A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 40.5 | 35.5 | 32.8 | 30.1 | 25.1 | 22.7 | 20.2 |
|  | 93 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 39.1 | 34.9 | 32.2 | 27.1 | 24.7 | 22.3 | 19.8 |
|  | 92 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 38.5 | 34.3 | 31.7 | 26.7 | 24.3 | 21.8 | 19.4 |
|  | 91 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 37.9 | 33.8 | 31.2 | 26.2 | 23.8 | 21.4 | 19.0 |
|  | 90 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 37.3 | 33.2 | 30.6 | 25.7 | 23.4 | 21.0 | 18.7 |



Bridge 220015, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 40.6 | 37.5 | 33.1 | 30.3 | 25.1 | 22.5 |
|  | 99 | \#N/A | SNS6A | SNS5A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 39.9 | 35.5 | 32.6 | 29.8 | 24.7 | 22.1 |
|  | 98 | \#N/A | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 39.3 | 34.9 | 32.1 | 26.9 | 24.3 | 21.7 |
|  | 97 | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 41.7 | 38.7 | 34.4 | 31.6 | 26.5 | 23.9 | 21.4 |
|  | 96 | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 41.1 | 38.1 | 33.9 | 31.1 | 26.0 | 23.5 | 21.0 |
|  | 95 | SNS7B | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 40.5 | 37.5 | 33.3 | 30.6 | 25.6 | 23.1 | 20.6 |
|  | 94 | SNS7B | SNS5A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 40.5 | 35.5 | 32.8 | 30.1 | 25.1 | 22.7 | 20.2 |
|  | 93 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 39.1 | 34.9 | 32.2 | 27.1 | 24.7 | 22.3 | 19.8 |
|  | 92 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 38.5 | 34.3 | 31.7 | 26.7 | 24.3 | 21.8 | 19.4 |
|  | 91 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 37.9 | 33.8 | 31.2 | 26.2 | 23.8 | 21.4 | 19.0 |
|  | 90 | SNS6A | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 37.3 | 33.2 | 30.6 | 25.7 | 23.4 | 21.0 | 18.7 |



Bridge 220015, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | N/A | 42.6 | 39.5 | 36.3 | 31.9 | 28.8 | 25.8 |
|  | 99 | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | N/A | 42.0 | 38.9 | 35.8 | 31.4 | 28.4 | 25.4 |
|  | 98 | TNAGT5B | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 44.4 | 41.4 | 38.3 | 35.2 | 30.9 | 27.9 | 24.9 |
|  | 97 | TNAGT5B | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 43.8 | 40.7 | 37.7 | 34.6 | 30.4 | 27.4 | 24.5 |
|  | 96 | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 43.1 | 40.1 | 37.1 | 32.7 | 29.8 | 26.9 | 24.0 |
|  | 95 | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 42.5 | 39.5 | 36.5 | 32.2 | 29.3 | 26.5 | 23.6 |
|  | 94 | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 42.5 | 38.9 | 35.9 | 31.7 | 28.8 | 26.0 | 23.2 |
|  | 93 | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 41.2 | 38.2 | 35.3 | 31.1 | 28.3 | 25.5 | 22.7 |
|  | 92 | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 40.5 | 37.6 | 34.8 | 30.6 | 27.8 | 25.0 | 22.3 |
|  | 91 | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 39.9 | 37.0 | 32.8 | 30.1 | 27.3 | 24.6 | 21.8 |
|  | 90 | TNAGT5B | TNAGT5B | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 39.2 | 36.4 | 32.2 | 29.5 | 26.8 | 24.1 | 21.4 |



Bridge 220015, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 33.2 | 30.9 | 25.4 | 23.3 | 21.2 | 19.1 | 17.0 |
|  | 99 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 32.7 | 27.1 | 25.0 | 22.9 | 20.8 | 18.8 | 16.7 |
|  | 98 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 32.3 | 26.7 | 24.6 | 22.6 | 20.5 | 18.4 | 16.4 |
|  | 97 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 31.8 | 26.3 | 24.2 | 22.2 | 20.2 | 18.1 | 16.1 |
|  | 96 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 31.3 | 25.9 | 23.9 | 21.8 | 19.8 | 17.8 | 15.8 |
|  | 95 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 30.8 | 25.5 | 23.5 | 21.5 | 19.5 | 17.5 | 15.5 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 27.0 | 25.1 | 23.1 | 21.1 | 19.1 | 17.1 | 15.2 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.6 | 24.7 | 22.7 | 20.7 | 18.8 | 16.8 | 14.9 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.2 | 24.2 | 22.3 | 20.4 | 18.4 | 16.5 | 14.6 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.7 | 23.8 | 21.9 | 20.0 | 18.1 | 16.2 | 14.3 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.3 | 23.4 | 21.5 | 19.6 | 17.7 | 15.8 | 14.0 |



Bridge 220025, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 33.2 | 30.9 | 25.4 | 23.3 | 21.2 | 19.1 | 17.0 |
|  | 99 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 32.7 | 27.1 | 25.0 | 22.9 | 20.8 | 18.8 | 16.7 |
|  | 98 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 32.3 | 26.7 | 24.6 | 22.6 | 20.5 | 18.4 | 16.4 |
|  | 97 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 31.8 | 26.3 | 24.2 | 22.2 | 20.2 | 18.1 | 16.1 |
|  | 96 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 31.3 | 25.9 | 23.9 | 21.8 | 19.8 | 17.8 | 15.8 |
|  | 95 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 30.8 | 25.5 | 23.5 | 21.5 | 19.5 | 17.5 | 15.5 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 27.0 | 25.1 | 23.1 | 21.1 | 19.1 | 17.1 | 15.2 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.6 | 24.7 | 22.7 | 20.7 | 18.8 | 16.8 | 14.9 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.2 | 24.2 | 22.3 | 20.4 | 18.4 | 16.5 | 14.6 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.7 | 23.8 | 21.9 | 20.0 | 18.1 | 16.2 | 14.3 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.3 | 23.4 | 21.5 | 19.6 | 17.7 | 15.8 | 14.0 |

RV Controlling Frequency, Single Unit Vehicles


Bridge 220025, Single Unit Vehicles


Bridge 220025, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 38.0 | 33.4 | 27.2 | 25.1 | 23.1 | 21.1 | 19.1 |
|  | 99 | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 35.2 | 32.9 | 26.8 | 24.8 | 22.8 | 20.8 | 18.8 |
|  | 98 | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 34.7 | 32.5 | 26.4 | 24.4 | 22.4 | 20.5 | 18.5 |
|  | 97 | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 34.2 | 32.0 | 26.0 | 24.1 | 22.1 | 20.2 | 18.2 |
|  | 96 | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 33.8 | 31.6 | 25.7 | 23.7 | 21.8 | 19.9 | 17.9 |
|  | 95 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 33.3 | 27.2 | 25.3 | 23.4 | 21.5 | 19.5 | 17.6 |
|  | 94 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 32.8 | 26.8 | 24.9 | 23.0 | 21.1 | 19.2 | 17.3 |
|  | 93 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 32.3 | 26.4 | 24.6 | 22.7 | 20.8 | 18.9 | 17.0 |
|  | 92 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 31.9 | 26.0 | 24.2 | 22.3 | 20.5 | 18.6 | 16.7 |
|  | 91 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 31.4 | 25.7 | 23.8 | 22.0 | 20.1 | 18.3 | 16.4 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 27.1 | 25.3 | 23.4 | 21.6 | 19.8 | 18.0 | 16.2 |



Bridge 240138, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 38.0 | 33.4 | 27.2 | 25.1 | 23.1 | 21.1 | 19.1 |
|  | 99 | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 35.2 | 32.9 | 26.8 | 24.8 | 22.8 | 20.8 | 18.8 |
|  | 98 | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 34.7 | 32.5 | 26.4 | 24.4 | 22.4 | 20.5 | 18.5 |
|  | 97 | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 34.2 | 32.0 | 26.0 | 24.1 | 22.1 | 20.2 | 18.2 |
|  | 96 | SNS5A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 33.8 | 31.6 | 25.7 | 23.7 | 21.8 | 19.9 | 17.9 |
|  | 95 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 33.3 | 27.2 | 25.3 | 23.4 | 21.5 | 19.5 | 17.6 |
|  | 94 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 32.8 | 26.8 | 24.9 | 23.0 | 21.1 | 19.2 | 17.3 |
|  | 93 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 32.3 | 26.4 | 24.6 | 22.7 | 20.8 | 18.9 | 17.0 |
|  | 92 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 31.9 | 26.0 | 24.2 | 22.3 | 20.5 | 18.6 | 16.7 |
|  | 91 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 31.4 | 25.7 | 23.8 | 22.0 | 20.1 | 18.3 | 16.4 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 27.1 | 25.3 | 23.4 | 21.6 | 19.8 | 18.0 | 16.2 |



Bridge 240138, Single Unit Vehicles


Bridge 240138, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.6 | 21.3 | 20.0 | 18.7 | 17.4 | 16.1 | 14.7 |
|  | 99 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.3 | 21.0 | 19.7 | 18.4 | 17.2 | 15.9 | 14.6 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.0 | 20.8 | 19.5 | 18.2 | 16.9 | 15.7 | 14.4 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 21.8 | 20.5 | 19.3 | 18.0 | 16.7 | 15.4 | 14.2 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 21.5 | 20.3 | 19.0 | 17.7 | 16.5 | 15.2 | 14.0 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 21.2 | 20.0 | 18.8 | 17.5 | 16.3 | 15.0 | 13.8 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 21.0 | 19.7 | 18.5 | 17.3 | 16.1 | 14.8 | 13.4 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 20.7 | 19.5 | 18.3 | 17.0 | 15.9 | 14.6 | 13.3 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 20.4 | 19.2 | 18.0 | 16.8 | 15.6 | 14.4 | 13.1 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 20.1 | 19.0 | 17.8 | 16.6 | 15.4 | 14.2 | 12.9 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 19.9 | 18.7 | 17.6 | 16.4 | 15.2 | 14.0 | 12.7 |



Bridge 310008, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.6 | 21.3 | 20.0 | 18.7 | 17.4 | 16.1 | 14.7 |
|  | 99 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.3 | 21.0 | 19.7 | 18.4 | 17.2 | 15.9 | 14.6 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 22.0 | 20.8 | 19.5 | 18.2 | 16.9 | 15.7 | 14.4 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 21.8 | 20.5 | 19.3 | 18.0 | 16.7 | 15.4 | 14.2 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 21.5 | 20.3 | 19.0 | 17.7 | 16.5 | 15.2 | 14.0 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 21.2 | 20.0 | 18.8 | 17.5 | 16.3 | 15.0 | 13.8 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 21.0 | 19.7 | 18.5 | 17.3 | 16.1 | 14.8 | 13.4 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 20.7 | 19.5 | 18.3 | 17.0 | 15.9 | 14.6 | 13.3 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 20.4 | 19.2 | 18.0 | 16.8 | 15.6 | 14.4 | 13.1 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 20.1 | 19.0 | 17.8 | 16.6 | 15.4 | 14.2 | 12.9 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 19.9 | 18.7 | 17.6 | 16.4 | 15.2 | 14.0 | 12.7 |

RV Controlling Frequency, Single Unit Vehicles


Bridge 310008, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 28.5 | 26.8 | 25.2 | 23.5 | 21.9 | 20.2 | 18.6 |
|  | 99 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 28.1 | 26.5 | 24.9 | 23.2 | 21.6 | 20.0 | 18.4 |
|  | 98 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 27.8 | 26.2 | 24.6 | 22.9 | 21.4 | 19.7 | 18.1 |
|  | 97 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 27.5 | 25.9 | 24.3 | 22.7 | 21.1 | 19.5 | 17.9 |
|  | 96 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 27.1 | 25.5 | 24.0 | 22.4 | 20.8 | 19.2 | 17.6 |
|  | 95 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 26.8 | 25.2 | 23.7 | 22.1 | 20.5 | 19.0 | 17.4 |
|  | 94 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 26.4 | 24.9 | 23.4 | 21.8 | 20.3 | 18.7 | 17.2 |
|  | 93 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 26.1 | 24.6 | 23.1 | 21.5 | 20.0 | 18.5 | 16.9 |
|  | 92 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 25.7 | 24.2 | 22.8 | 21.2 | 19.7 | 18.2 | 16.7 |
|  | 91 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 25.4 | 23.9 | 22.5 | 20.9 | 19.5 | 18.0 | 16.5 |
|  | 90 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 25.1 | 23.6 | 22.1 | 20.6 | 19.2 | 17.7 | 16.2 |



Bridge 310008, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 20.7 | 19.5 | 18.3 | 17.1 | 16.0 | 14.8 | 13.4 |
|  | 99 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 20.4 | 19.3 | 18.1 | 16.9 | 15.8 | 14.6 | 13.2 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 20.2 | 19.0 | 17.9 | 16.7 | 15.6 | 14.4 | 13.0 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 19.9 | 18.8 | 17.7 | 16.5 | 15.4 | 14.3 | 12.9 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 19.7 | 18.6 | 17.5 | 16.3 | 15.2 | 14.1 | 12.7 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 19.5 | 18.3 | 17.2 | 16.1 | 15.0 | 13.9 | 12.5 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 19.2 | 18.1 | 17.0 | 15.9 | 14.8 | 13.7 | 12.4 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 19.0 | 17.9 | 16.8 | 15.7 | 14.6 | 13.3 | 12.2 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 18.7 | 17.7 | 16.6 | 15.5 | 14.4 | 13.1 | 12.1 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 18.5 | 17.4 | 16.4 | 15.3 | 14.2 | 12.9 | 11.9 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 18.3 | 17.2 | 16.2 | 15.1 | 14.0 | 12.8 | 11.7 |



Bridge 310089, All Vehicles


Bridge 310089, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 27.1 | 25.6 | 24.0 | 22.5 | 20.9 | 19.4 | 17.9 |
|  | 99 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 26.8 | 25.3 | 23.8 | 22.2 | 20.7 | 19.2 | 17.6 |
|  | 98 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 26.5 | 25.0 | 23.5 | 22.0 | 20.4 | 18.9 | 17.4 |
|  | 97 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 26.2 | 24.7 | 23.2 | 21.7 | 20.2 | 18.7 | 17.2 |
|  | 96 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 25.8 | 24.4 | 22.9 | 21.4 | 19.9 | 18.5 | 17.0 |
|  | 95 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 25.5 | 24.1 | 22.6 | 21.2 | 19.7 | 18.2 | 16.8 |
|  | 94 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 25.2 | 23.8 | 22.3 | 20.9 | 19.4 | 18.0 | 16.5 |
|  | 93 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 24.9 | 23.5 | 22.1 | 20.6 | 19.2 | 17.8 | 16.3 |
|  | 92 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 24.6 | 23.2 | 21.8 | 20.3 | 18.9 | 17.5 | 16.1 |
|  | 91 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 24.3 | 22.9 | 21.5 | 20.1 | 18.7 | 17.3 | 15.9 |
|  | 90 | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 24.0 | 22.6 | 21.2 | 19.8 | 18.4 | 17.1 | 15.7 |



Bridge 310089, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | 38.1 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 41.4 | 35.4 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 40.8 | 34.9 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 40.3 | 34.4 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 39.5 | 33.9 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 39.0 | 33.4 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 38.4 | 32.9 |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.5 | 37.8 | 32.4 |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.8 | 35.1 | 31.9 |
|  | 91 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.2 | 34.5 | 31.4 |
|  | 90 | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 39.4 | 34.0 | 30.9 |

RV Controlling Frequency, All Vehicles


Bridge 330276, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
| Кวиә!э!ษヨ әรр!ィя | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | 38.1 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 41.4 | 35.4 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 40.8 | 34.9 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 40.3 | 34.4 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 39.5 | 33.9 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 39.0 | 33.4 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 38.4 | 32.9 |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.5 | 37.8 | 32.4 |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.8 | 35.1 | 31.9 |
|  | 91 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.2 | 34.5 | 31.4 |
|  | 90 | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 39.4 | 34.0 | 30.9 |

RV Controlling Frequency, Single Unit Vehicles


Bridge 330276, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | N/A | 41.1 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 44.5 | 40.6 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 43.9 | 40.0 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 43.3 | 39.4 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 42.7 | 38.9 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 42.0 | 38.3 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 41.4 | 37.7 |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 44.5 | 40.8 | 37.2 |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 43.9 | 40.2 | 36.6 |
|  | 91 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 43.2 | 39.6 | 36.0 |
|  | 90 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 42.6 | 39.0 | 35.5 |

RV Controlling Frequency, Tandem Trucks


Bridge 330276, Tandem Trucks


Bridge 350022, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | SNS6A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | N/A | 37.9 | 27.2 | 25.3 | 23.5 | 21.6 | 19.7 |
|  | 99 | SNS7B | SNS6A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 41.7 | 37.9 | 26.8 | 25.0 | 23.1 | 21.3 | 19.4 |
|  | 98 | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 39.8 | 35.5 | 26.5 | 24.7 | 22.8 | 21.0 | 19.2 |
|  | 97 | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 39.3 | 35.0 | 26.2 | 24.3 | 22.5 | 20.7 | 18.9 |
|  | 96 | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 38.8 | 34.6 | 25.8 | 24.0 | 22.2 | 20.4 | 18.6 |
|  | 95 | SNS6A | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 38.3 | 34.1 | 25.5 | 23.7 | 21.9 | 20.1 | 18.4 |
|  | 94 | SNS6A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 37.8 | 26.9 | 25.1 | 23.4 | 21.6 | 19.9 | 18.1 |
|  | 93 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 35.4 | 26.5 | 24.8 | 23.0 | 21.3 | 19.6 | 17.8 |
|  | 92 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 34.9 | 26.2 | 24.5 | 22.7 | 21.0 | 19.3 | 17.6 |
|  | 91 | SNS5A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 34.4 | 25.8 | 24.1 | 22.4 | 20.7 | 19.0 | 17.3 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 27.1 | 25.5 | 23.8 | 22.1 | 20.4 | 18.7 | 17.0 |



Bridge 350022, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A |
|  |  | N/A | N/A | 40.5 | 37.7 | 31.4 | 28.8 | 26.3 |
|  | 99 | \#N/A | \#N/A | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A |
|  |  | N/A | N/A | 40.0 | 37.2 | 31.0 | 28.5 | 26.0 |
|  | 98 | \#N/A | \#N/A | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | N/A | N/A | 39.5 | 33.0 | 30.5 | 28.1 | 25.6 |
|  | 97 | \#N/A | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | N/A | 41.7 | 39.0 | 32.5 | 30.1 | 27.7 | 25.3 |
|  | 96 | \#N/A | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | N/A | 41.2 | 38.5 | 32.1 | 29.7 | 27.3 | 24.9 |
|  | 95 | \#N/A | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | N/A | 40.6 | 38.0 | 31.7 | 29.3 | 26.9 | 24.6 |
|  | 94 | \#N/A | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | N/A | 40.1 | 37.4 | 31.2 | 28.9 | 26.6 | 24.2 |
|  | 93 | \#N/A | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | N/A | 39.5 | 36.9 | 30.8 | 28.5 | 26.2 | 23.8 |
|  | 92 | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 41.6 | 39.0 | 32.7 | 30.4 | 28.1 | 25.8 | 23.5 |
|  | 91 | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 41.0 | 38.5 | 32.2 | 30.0 | 27.7 | 25.4 | 23.1 |
|  | 90 | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 40.4 | 37.9 | 31.8 | 29.5 | 27.3 | 25.0 | 22.8 |



Bridge 350022, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A |
|  |  | N/A | N/A | N/A | N/A | N/A | 41.1 | 37.8 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A |
|  |  | N/A | N/A | N/A | N/A | N/A | 40.6 | 37.3 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 40.1 | 35.3 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 44.9 | 39.5 | 34.9 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 44.4 | 39.0 | 34.4 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.7 | 38.5 | 34.0 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.1 | 38.0 | 33.6 |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.6 | 37.5 | 33.1 |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.1 | 35.5 | 32.7 |
|  | 91 | \#N/A | \#N/A | \#N/A | TNAGT5B | SNS6A | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | 44.6 | 39.4 | 35.0 | 32.2 |
|  | 90 | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | 41.9 | 38.9 | 34.5 | 31.8 |

RV Controlling Frequency, All Vehicles


Bridge 430003, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A |
|  |  | N/A | N/A | N/A | N/A | N/A | 41.1 | 37.8 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A |
|  |  | N/A | N/A | N/A | N/A | N/A | 40.6 | 37.3 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 40.1 | 35.3 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 39.5 | 34.9 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 39.0 | 34.4 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.7 | 38.5 | 34.0 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.1 | 38.0 | 33.6 |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.6 | 37.5 | 33.1 |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.1 | 35.5 | 32.7 |
|  | 91 | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 39.4 | 35.0 | 32.2 |
|  | 90 | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | 41.9 | 38.9 | 34.5 | 31.8 |

RV Controlling Frequency, Single Unit Vehicles


Bridge 430003, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 43.3 | 39.9 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 42.7 | 39.4 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 42.2 | 38.9 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 44.9 | 41.7 | 38.4 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 44.4 | 41.2 | 37.9 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 43.8 | 40.6 | 37.4 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 43.3 | 40.1 | 37.0 |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 42.7 | 39.6 | 36.5 |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 42.2 | 39.1 | 36.0 |
|  | 91 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | 44.6 | 41.6 | 38.5 | 35.5 |
|  | 90 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | 44.1 | 41.0 | 38.0 | 35.0 |



Bridge 430003, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 27.1 | 25.0 | 22.9 | 20.8 | 18.6 | 16.5 | 14.4 |
|  | 99 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.7 | 24.6 | 22.5 | 20.4 | 18.3 | 16.2 | 14.1 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.3 | 24.2 | 22.1 | 20.0 | 17.9 | 15.8 | 13.7 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 25.8 | 23.7 | 21.7 | 19.6 | 17.6 | 15.5 | 13.4 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 25.4 | 23.3 | 21.3 | 19.2 | 17.2 | 15.2 | 13.1 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 24.9 | 22.9 | 20.9 | 18.9 | 16.9 | 14.8 | 12.7 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 24.5 | 22.5 | 20.5 | 18.5 | 16.5 | 14.5 | 12.4 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 24.0 | 22.1 | 20.1 | 18.1 | 16.1 | 14.2 | 12.1 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 23.6 | 21.6 | 19.7 | 17.7 | 15.8 | 13.8 | 11.8 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTSS | SNCOTTS3 | SNSH | SNSH |
|  |  | 23.2 | 21.2 | 19.3 | 17.4 | 15.4 | 13.4 | 11.5 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 22.7 | 20.8 | 18.9 | 17.0 | 15.1 | 13.1 | 11.2 |



Bridge 480189, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 27.1 | 25.0 | 22.9 | 20.8 | 18.6 | 16.5 | 14.4 |
|  | 99 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.7 | 24.6 | 22.5 | 20.4 | 18.3 | 16.2 | 14.1 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.3 | 24.2 | 22.1 | 20.0 | 17.9 | 15.8 | 13.7 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 25.8 | 23.7 | 21.7 | 19.6 | 17.6 | 15.5 | 13.4 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 25.4 | 23.3 | 21.3 | 19.2 | 17.2 | 15.2 | 13.1 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 24.9 | 22.9 | 20.9 | 18.9 | 16.9 | 14.8 | 12.7 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 24.5 | 22.5 | 20.5 | 18.5 | 16.5 | 14.5 | 12.4 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 24.0 | 22.1 | 20.1 | 18.1 | 16.1 | 14.2 | 12.1 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH |
|  |  | 23.6 | 21.6 | 19.7 | 17.7 | 15.8 | 13.8 | 11.8 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 23.2 | 21.2 | 19.3 | 17.4 | 15.4 | 13.4 | 11.5 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNSH | SNSH |
|  |  | 22.7 | 20.8 | 18.9 | 17.0 | 15.1 | 13.1 | 11.2 |

RV Controlling Frequency, Single Unit Vehicles


Bridge 480189, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 31.1 | 28.6 | 26.2 | 23.8 | 21.3 | 18.9 | 16.5 |
|  | 99 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 30.6 | 28.2 | 25.8 | 23.3 | 20.9 | 18.5 | 16.1 |
|  | 98 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 30.1 | 27.7 | 25.3 | 22.9 | 20.5 | 18.1 | 15.7 |
|  | 97 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 29.6 | 27.2 | 24.8 | 22.5 | 20.1 | 17.7 | 15.4 |
|  | 96 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 29.1 | 26.7 | 24.4 | 22.0 | 19.7 | 17.4 | 15.0 |
|  | 95 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 28.6 | 26.2 | 23.9 | 21.6 | 19.3 | 17.0 | 14.7 |
|  | 94 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 28.0 | 25.8 | 23.5 | 21.2 | 18.9 | 16.6 | 14.3 |
|  | 93 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 27.5 | 25.3 | 23.0 | 20.7 | 18.5 | 16.2 | 14.0 |
|  | 92 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 27.0 | 24.8 | 22.6 | 20.3 | 18.1 | 15.8 | 13.6 |
|  | 91 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 26.5 | 24.3 | 22.1 | 19.9 | 17.7 | 15.5 | 13.3 |
|  | 90 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 | TNAGRIT3 |
|  |  | 26.0 | 23.8 | 21.6 | 19.5 | 17.3 | 15.1 | 12.9 |



Bridge 480189, Tandem Trucks

| All Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNS6A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 39.3 | 26.2 | 24.8 | 23.3 | 21.7 | 20.3 | 18.8 |
|  | 99 | SNS6A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 38.9 | 26.0 | 24.5 | 23.1 | 21.5 | 20.1 | 18.6 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 27.1 | 25.7 | 24.2 | 22.8 | 21.3 | 19.8 | 18.4 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.8 | 25.4 | 24.0 | 22.5 | 21.0 | 19.6 | 18.2 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.5 | 25.1 | 23.7 | 22.3 | 20.8 | 19.4 | 17.9 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.2 | 24.8 | 23.4 | 22.0 | 20.5 | 19.1 | 17.7 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.9 | 24.5 | 23.1 | 21.8 | 20.3 | 18.9 | 17.5 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.6 | 24.2 | 22.9 | 21.5 | 20.0 | 18.7 | 17.3 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.3 | 23.9 | 22.6 | 21.2 | 19.8 | 18.5 | 17.1 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.0 | 23.7 | 22.3 | 21.0 | 19.6 | 18.2 | 16.9 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 24.7 | 23.4 | 22.0 | 20.7 | 19.3 | 18.0 | 16.7 |



Bridge 490054, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNS6A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 39.3 | 26.2 | 24.8 | 23.3 | 21.7 | 20.3 | 18.8 |
|  | 99 | SNS6A | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 38.9 | 26.0 | 24.5 | 23.1 | 21.5 | 20.1 | 18.6 |
|  | 98 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 27.1 | 25.7 | 24.2 | 22.8 | 21.3 | 19.8 | 18.4 |
|  | 97 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.8 | 25.4 | 24.0 | 22.5 | 21.0 | 19.6 | 18.2 |
|  | 96 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.5 | 25.1 | 23.7 | 22.3 | 20.8 | 19.4 | 17.9 |
|  | 95 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 26.2 | 24.8 | 23.4 | 22.0 | 20.5 | 19.1 | 17.7 |
|  | 94 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.9 | 24.5 | 23.1 | 21.8 | 20.3 | 18.9 | 17.5 |
|  | 93 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.6 | 24.2 | 22.9 | 21.5 | 20.0 | 18.7 | 17.3 |
|  | 92 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.3 | 23.9 | 22.6 | 21.2 | 19.8 | 18.5 | 17.1 |
|  | 91 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 25.0 | 23.7 | 22.3 | 21.0 | 19.6 | 18.2 | 16.9 |
|  | 90 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 | SNCOTTS3 |
|  |  | 24.7 | 23.4 | 22.0 | 20.7 | 19.3 | 18.0 | 16.7 |

RV Controlling Frequency, Single Unit Vehicles


Bridge 490054, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | TNT7B | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A |
|  |  | N/A | 40.8 | 38.5 | 36.2 | 30.9 | 28.8 | 26.7 |
|  | 99 | \#N/A | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | N/A | 40.3 | 38.1 | 32.8 | 30.6 | 28.5 | 26.4 |
|  | 98 | \#N/A | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | N/A | 39.9 | 37.7 | 32.4 | 30.2 | 28.2 | 26.1 |
|  | 97 | TNT7B | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 41.7 | 39.4 | 37.2 | 32.0 | 29.9 | 27.9 | 25.8 |
|  | 96 | TNT7B | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 41.2 | 39.0 | 36.8 | 31.7 | 29.5 | 27.5 | 25.5 |
|  | 95 | TNT7B | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 40.8 | 38.5 | 36.4 | 31.3 | 29.2 | 27.2 | 25.2 |
|  | 94 | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 40.3 | 38.1 | 32.9 | 30.9 | 28.8 | 26.9 | 24.9 |
|  | 93 | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 39.8 | 37.7 | 32.5 | 30.6 | 28.5 | 26.6 | 24.6 |
|  | 92 | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 39.4 | 37.2 | 32.1 | 30.2 | 28.2 | 26.2 | 24.3 |
|  | 91 | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 38.9 | 36.8 | 31.7 | 29.8 | 27.8 | 25.9 | 24.0 |
|  | 90 | TNT7B | TNT7B | TNT4A | TNT4A | TNT4A | TNT4A | TNT4A |
|  |  | 38.4 | 36.3 | 31.3 | 29.5 | 27.5 | 25.6 | 23.7 |



Bridge 490054, Tandem Trucks


Bridge 590054, All Vehicles

| Single Unit Vehicles |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 40.8 | 34.9 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 40.2 | 34.3 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 39.4 | 33.7 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | N/A | 38.7 | 33.1 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 41.6 | 38.1 | 32.6 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.9 | 35.1 | 32.0 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A |
|  |  | N/A | N/A | N/A | N/A | 40.2 | 34.5 | 31.4 |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | N/A | 39.4 | 33.9 | 27.0 |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | SNS6A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | N/A | 38.7 | 33.3 | 26.5 |
|  | 91 | \#N/A | \#N/A | \#N/A | SNS7B | SNS6A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 41.3 | 38.0 | 32.7 | 26.0 |
|  | 90 | \#N/A | \#N/A | \#N/A | SNS7B | SNS5A | SNS5A | SNCOTTS3 |
|  |  | N/A | N/A | N/A | 40.6 | 35.0 | 32.1 | 25.5 |

RV Controlling Frequency, Single Unit Vehicles


Bridge 590054, Single Unit Vehicles

| Tandem Trucks |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rating Vehicle |  | Section Loss |  |  |  |  |  |  |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 44.1 | 40.3 |
|  | 99 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 43.4 | 39.7 |
|  | 98 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 42.7 | 39.0 |
|  | 97 | \#N/A | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | N/A | 42.0 | 38.3 |
|  | 96 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 44.9 | 41.3 | 37.7 |
|  | 95 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 44.2 | 40.6 | 37.0 |
|  | 94 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 43.5 | 39.9 | 36.3 |
|  | 93 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B |
|  |  | N/A | N/A | N/A | N/A | 42.7 | 39.2 | 35.7 |
|  | 92 | \#N/A | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGRIT3 |
|  |  | N/A | N/A | N/A | N/A | 42.0 | 38.5 | 32.8 |
|  | 91 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 |
|  |  | N/A | N/A | N/A | 44.6 | 41.2 | 37.8 | 32.2 |
|  | 90 | \#N/A | \#N/A | \#N/A | TNAGT5B | TNAGT5B | TNAGT5B | TNAGRIT3 |
|  |  | N/A | N/A | N/A | 43.8 | 40.5 | 37.1 | 31.6 |



Bridge 590054, Tandem Trucks

Group 1 Bridges, Critical Vehicles:

|  |  |  |  |  | tion L |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 21.8 | 20.2 | 18.6 | 17.0 | 15.4 | 13.7 | 12.1 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 21.5 | 19.9 | 18.3 | 16.7 | 15.1 | 13.5 | 11.9 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 21.2 | 19.6 | 18.0 | 16.4 | 14.8 | 13.2 | 11.7 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 20.8 | 19.3 | 17.7 | 16.1 | 14.6 | 13.0 | 11.4 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 20.5 | 19.0 | 17.4 | 15.8 | 14.3 | 12.7 | 11.2 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 20.2 | 18.6 | 17.1 | 15.6 | 14.0 | 12.5 | 11.0 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 19.9 | 18.3 | 16.8 | 15.3 | 13.8 | 12.2 | 10.7 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 19.5 | 18.0 | 16.5 | 15.0 | 13.5 | 12.0 | 10.5 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 19.2 | 17.7 | 16.2 | 14.7 | 13.2 | 11.8 | 10.3 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 18.9 | 17.4 | 15.9 | 14.4 | 13.0 | 11.5 | 10.0 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 18.5 | 17.1 | 15.6 | 14.2 | 12.7 | 11.3 | 9.8 |

Bridge 010003

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 44.4 | 41.7 | 39.0 | 36.3 | 33.6 | 30.9 | 28.2 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 43.8 | 41.2 | 38.5 | 35.8 | 33.1 | 30.5 | 27.8 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 43.3 | 40.6 | 38.0 | 35.3 | 32.7 | 30.1 | 27.4 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 42.7 | 40.1 | 37.5 | 34.9 | 32.3 | 29.7 | 27.0 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 42.2 | 39.6 | 37.0 | 34.4 | 31.8 | 29.2 | 26.6 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 41.6 | 39.1 | 36.5 | 33.9 | 31.4 | 28.8 | 26.2 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 41.1 | 38.5 | 36.0 | 33.5 | 30.9 | 28.4 | 25.9 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 40.5 | 38.0 | 35.5 | 33.0 | 30.5 | 28.0 | 25.5 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 40.0 | 37.5 | 35.0 | 32.5 | 30.1 | 27.6 | 25.1 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 39.4 | 37.0 | 34.5 | 32.1 | 29.6 | 27.2 | 24.7 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 38.9 | 36.4 | 34.0 | 31.6 | 29.2 | 26.8 | 24.3 |

Bridge 080037

|  |  |  |  |  | tion L |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 55.9 | 52.9 | 50.0 | 47.0 | 44.0 | 41.0 | 38.0 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 55.3 | 52.4 | 49.4 | 46.5 | 43.5 | 40.6 | 37.6 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 54.7 | 51.8 | 48.9 | 46.0 | 43.0 | 40.1 | 37.2 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 54.1 | 51.2 | 48.3 | 45.5 | 42.5 | 39.7 | 36.8 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 53.5 | 50.6 | 47.8 | 44.9 | 42.1 | 39.2 | 36.3 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 52.9 | 50.0 | 47.2 | 43.9 | 41.6 | 38.7 | 35.9 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 52.3 | 49.5 | 46.7 | 43.9 | 41.1 | 38.3 | 35.5 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 51.7 | 48.9 | 46.1 | 43.4 | 40.6 | 37.8 | 35.1 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 51.0 | 48.3 | 45.6 | 42.9 | 40.1 | 37.4 | 34.6 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 50.4 | 47.7 | 45.0 | 42.3 | 39.6 | 36.9 | 34.2 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 49.8 | 47.1 | 44.5 | 41.8 | 39.1 | 36.5 | 33.8 |

Bridge 100152

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 24.5 | 23.2 | 21.8 | 20.5 | 19.1 | 17.8 | 16.4 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 24.2 | 22.9 | 21.6 | 20.3 | 18.9 | 17.6 | 16.2 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 24.0 | 22.7 | 21.3 | 20.0 | 18.7 | 17.4 | 16.0 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 23.7 | 22.4 | 21.1 | 19.8 | 18.5 | 17.2 | 15.8 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 23.4 | 22.1 | 20.8 | 19.6 | 18.2 | 16.9 | 15.6 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 23.1 | 21.9 | 20.6 | 19.3 | 18.0 | 16.7 | 15.4 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 22.9 | 21.6 | 20.4 | 19.1 | 17.8 | 16.5 | 15.2 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 22.6 | 21.3 | 20.1 | 18.9 | 17.6 | 16.3 | 15.1 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 22.3 | 21.1 | 19.9 | 18.6 | 17.4 | 16.1 | 14.9 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 22.0 | 20.8 | 19.6 | 18.4 | 17.1 | 15.9 | 14.7 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 21.8 | 20.6 | 19.4 | 18.2 | 16.9 | 15.7 | 14.5 |

Bridge 100309

|  |  |  |  |  | tion L |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 40.8 | 38.0 | 35.2 | 32.5 | 29.7 | 27.0 | 24.2 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 40.2 | 37.5 | 34.7 | 32.0 | 29.3 | 26.5 | 23.8 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 39.6 | 37.0 | 34.2 | 31.5 | 28.8 | 26.1 | 23.4 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 39.1 | 36.4 | 33.7 | 31.0 | 28.4 | 25.7 | 23.0 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 38.5 | 35.9 | 33.2 | 30.5 | 27.9 | 25.3 | 22.6 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 37.9 | 35.4 | 32.7 | 30.1 | 27.5 | 24.9 | 22.2 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 37.4 | 34.8 | 32.2 | 29.6 | 27.0 | 24.4 | 21.8 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 36.8 | 34.3 | 31.7 | 29.1 | 26.6 | 24.0 | 21.4 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 36.3 | 33.7 | 31.2 | 28.6 | 26.1 | 23.6 | 21.0 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 35.7 | 33.2 | 30.7 | 28.2 | 25.7 | 23.2 | 20.6 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 35.1 | 32.7 | 30.2 | 27.7 | 25.2 | 22.7 | 20.2 |

Bridge 110105

|  |  |  |  |  | tion L |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 38.1 | 35.4 | 32.8 | 30.2 | 27.6 | 25.0 | 22.4 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 37.5 | 34.9 | 32.3 | 29.7 | 27.2 | 24.6 | 22.0 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 37.0 | 34.4 | 31.8 | 29.3 | 26.7 | 24.2 | 21.6 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 36.4 | 33.9 | 31.4 | 28.8 | 26.3 | 23.7 | 21.2 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 35.9 | 33.4 | 30.9 | 28.4 | 25.9 | 23.3 | 20.8 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 35.3 | 32.9 | 30.4 | 27.9 | 25.4 | 22.9 | 20.5 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 35.3 | 32.3 | 29.9 | 27.4 | 25.0 | 22.5 | 20.1 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 34.2 | 31.8 | 29.4 | 27.0 | 24.5 | 22.1 | 19.7 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 33.7 | 31.3 | 28.9 | 26.5 | 24.1 | 21.7 | 19.3 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 33.2 | 30.8 | 28.4 | 26.0 | 23.7 | 21.3 | 18.9 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 32.6 | 30.3 | 27.9 | 25.6 | 23.2 | 20.9 | 18.5 |

Bridge 220015

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 29.3 | 27.3 | 25.2 | 23.1 | 21.0 | 18.9 | 16.8 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 28.9 | 26.9 | 24.8 | 22.7 | 20.7 | 18.6 | 16.5 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 28.5 | 26.5 | 24.4 | 22.4 | 20.3 | 18.3 | 16.2 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 28.1 | 26.0 | 24.0 | 22.0 | 20.0 | 17.9 | 15.9 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 27.6 | 25.6 | 23.6 | 21.6 | 19.6 | 17.6 | 15.6 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 27.2 | 25.2 | 23.2 | 21.3 | 19.3 | 17.3 | 15.3 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 26.8 | 24.8 | 22.9 | 20.9 | 18.9 | 17.0 | 15.0 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 26.3 | 24.4 | 22.5 | 20.5 | 18.6 | 16.7 | 14.7 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 25.9 | 24.0 | 22.1 | 20.2 | 18.3 | 16.3 | 14.4 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 25.5 | 23.6 | 21.7 | 19.8 | 17.9 | 16.0 | 14.1 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 25.1 | 23.2 | 21.3 | 19.4 | 17.6 | 15.7 | 13.8 |

Bridge 220025

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 30.8 | 28.9 | 26.8 | 24.9 | 22.8 | 20.9 | 18.8 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 30.4 | 28.5 | 26.5 | 24.5 | 22.5 | 20.5 | 18.6 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 30.0 | 28.1 | 26.1 | 24.2 | 22.2 | 20.2 | 18.3 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 29.6 | 27.7 | 25.7 | 23.8 | 21.9 | 19.9 | 18.0 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 29.2 | 27.3 | 25.4 | 23.5 | 21.5 | 19.6 | 17.7 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 28.8 | 26.9 | 25.0 | 23.1 | 21.2 | 19.3 | 17.4 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 28.4 | 26.5 | 24.6 | 22.8 | 20.9 | 19.0 | 17.1 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 28.0 | 26.1 | 24.3 | 22.4 | 20.6 | 18.7 | 16.8 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 27.6 | 25.7 | 23.9 | 22.1 | 20.2 | 18.4 | 16.5 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 27.2 | 25.4 | 23.5 | 21.7 | 19.9 | 18.1 | 16.3 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 26.7 | 25.0 | 23.2 | 21.4 | 19.6 | 17.8 | 16.0 |

Bridge 240138

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 22.3 | 21.0 | 19.7 | 18.4 | 17.1 | 15.8 | 14.6 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 22.0 | 20.7 | 19.5 | 18.2 | 16.9 | 15.6 | 14.4 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 21.7 | 20.5 | 19.2 | 18.0 | 16.7 | 15.4 | 14.2 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 21.5 | 20.2 | 19.0 | 17.7 | 16.5 | 15.2 | 14.0 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 21.2 | 20.0 | 18.8 | 17.5 | 16.3 | 15.0 | 13.8 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 20.9 | 19.7 | 18.5 | 17.3 | 16.1 | 14.8 | 13.6 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 20.7 | 19.5 | 18.3 | 17.0 | 15.9 | 14.6 | 13.4 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 20.4 | 19.2 | 18.0 | 16.8 | 15.6 | 14.4 | 13.3 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 20.1 | 19.0 | 17.8 | 16.6 | 15.4 | 14.2 | 13.1 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 19.9 | 18.7 | 17.6 | 16.4 | 15.2 | 14.0 | 12.9 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 19.6 | 18.5 | 17.3 | 16.1 | 15.0 | 13.8 | 12.7 |

Bridge 310008

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 20.3 | 19.1 | 18.0 | 16.8 | 15.7 | 14.5 | 13.4 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 20.0 | 18.9 | 17.8 | 16.6 | 15.5 | 14.4 | 13.2 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 19.8 | 18.7 | 17.6 | 16.4 | 15.3 | 14.2 | 13.0 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 19.6 | 18.4 | 17.4 | 16.2 | 15.1 | 14.0 | 12.9 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 19.3 | 18.2 | 17.1 | 16.0 | 14.9 | 13.8 | 12.7 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 19.1 | 18.0 | 16.9 | 15.8 | 14.7 | 13.6 | 12.5 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 18.9 | 17.8 | 16.7 | 15.6 | 14.5 | 13.5 | 12.4 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 18.6 | 17.6 | 16.5 | 15.4 | 14.3 | 13.3 | 12.2 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 18.4 | 17.3 | 16.3 | 15.2 | 14.2 | 13.1 | 12.1 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 18.2 | 17.1 | 16.1 | 15.0 | 14.0 | 12.9 | 11.9 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 17.9 | 16.9 | 15.9 | 14.8 | 13.8 | 12.8 | 11.7 |

Bridge 310089

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 49.4 | 46.4 | 43.4 | 40.4 | 37.3 | 34.3 | 31.3 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 48.8 | 45.8 | 42.8 | 39.8 | 36.9 | 33.9 | 30.9 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 48.2 | 45.2 | 42.3 | 39.3 | 36.4 | 33.4 | 30.4 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 47.6 | 44.7 | 41.7 | 38.8 | 35.9 | 32.9 | 30.0 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 47.0 | 44.1 | 41.2 | 38.3 | 35.4 | 32.5 | 29.6 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 46.4 | 43.5 | 40.6 | 37.7 | 34.9 | 32.0 | 29.1 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 45.7 | 42.9 | 40.1 | 37.2 | 34.4 | 31.5 | 28.7 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 45.1 | 42.3 | 39.5 | 36.7 | 33.9 | 31.1 | 28.3 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 44.5 | 41.7 | 39.0 | 36.2 | 33.4 | 30.6 | 27.8 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 43.9 | 41.1 | 38.4 | 35.6 | 32.9 | 30.1 | 27.4 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 43.3 | 40.5 | 37.8 | 35.1 | 32.4 | 29.7 | 27.0 |

Bridge 330276

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 29.7 | 27.5 | 26.1 | 24.3 | 22.5 | 20.7 | 18.9 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 29.3 | 27.5 | 25.8 | 24.0 | 22.2 | 20.4 | 18.6 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 29.0 | 27.2 | 25.4 | 23.7 | 21.9 | 20.1 | 18.4 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 28.6 | 26.8 | 25.1 | 23.3 | 21.6 | 19.9 | 18.1 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 28.2 | 26.5 | 24.8 | 23.0 | 21.3 | 19.6 | 17.9 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 27.9 | 26.2 | 24.4 | 22.7 | 21.0 | 19.3 | 17.6 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 27.5 | 25.8 | 24.1 | 22.4 | 20.7 | 19.1 | 17.4 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 27.1 | 25.5 | 23.8 | 22.1 | 20.5 | 18.8 | 17.1 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 26.8 | 25.1 | 23.5 | 21.8 | 20.2 | 18.5 | 16.8 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 26.4 | 24.8 | 23.1 | 21.5 | 19.9 | 18.2 | 16.6 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 26.0 | 24.4 | 22.8 | 21.2 | 19.6 | 18.0 | 16.3 |

Bridge 350022

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 49.4 | 46.7 | 43.9 | 41.1 | 38.3 | 35.6 | 32.8 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 48.9 | 46.1 | 43.4 | 40.6 | 37.9 | 35.1 | 32.4 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 48.3 | 45.6 | 42.9 | 40.1 | 37.4 | 34.7 | 32.0 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 47.7 | 45.0 | 42.4 | 39.7 | 37.0 | 34.3 | 31.6 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 47.1 | 44.5 | 41.8 | 39.2 | 36.5 | 33.9 | 31.2 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 46.6 | 43.9 | 41.3 | 38.7 | 36.1 | 33.4 | 30.8 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 46.0 | 43.4 | 40.8 | 38.2 | 35.6 | 33.0 | 30.4 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 45.4 | 42.8 | 40.3 | 37.7 | 35.1 | 32.6 | 30.0 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 44.8 | 42.3 | 39.8 | 37.2 | 34.7 | 32.1 | 29.6 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 44.3 | 41.7 | 39.3 | 36.7 | 34.2 | 31.7 | 29.2 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 43.7 | 41.2 | 38.7 | 36.2 | 33.8 | 31.3 | 28.8 |

Bridge 430003

|  |  |  |  |  | tion L |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 27.0 | 24.8 | 22.7 | 20.6 | 18.5 | 16.4 | 14.3 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 26.5 | 24.4 | 22.3 | 20.3 | 18.2 | 16.1 | 14.0 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 26.1 | 24.0 | 21.9 | 19.9 | 17.8 | 15.7 | 13.7 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 25.6 | 23.6 | 21.5 | 19.5 | 17.5 | 15.4 | 13.4 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 25.2 | 23.2 | 21.2 | 19.1 | 17.1 | 15.1 | 13.1 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 24.8 | 22.8 | 20.8 | 18.8 | 16.8 | 14.7 | 12.7 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 24.3 | 22.3 | 20.4 | 18.4 | 16.4 | 14.4 | 12.4 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 23.9 | 21.9 | 20.0 | 18.0 | 16.0 | 14.1 | 12.1 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 23.4 | 21.5 | 19.6 | 17.6 | 15.7 | 13.8 | 11.8 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 23.0 | 21.1 | 19.2 | 17.3 | 15.3 | 13.4 | 11.5 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 22.6 | 20.7 | 18.8 | 16.9 | 15.0 | 13.1 | 11.2 |

## Bridge 480189

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 25.1 | 23.8 | 22.4 | 21.1 | 19.7 | 18.4 | 17.0 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 24.9 | 23.5 | 22.2 | 20.9 | 19.5 | 18.2 | 16.8 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 24.6 | 23.3 | 21.9 | 20.6 | 19.3 | 18.0 | 16.6 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 24.3 | 23.0 | 21.7 | 20.4 | 19.0 | 17.7 | 16.4 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 24.0 | 22.7 | 21.5 | 20.2 | 18.8 | 17.5 | 16.3 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 23.8 | 22.5 | 21.2 | 19.9 | 18.6 | 17.3 | 16.1 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 23.5 | 22.2 | 21.0 | 19.7 | 18.4 | 17.1 | 15.9 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 23.2 | 21.9 | 20.7 | 19.5 | 18.2 | 16.9 | 15.7 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 22.9 | 21.7 | 20.5 | 19.2 | 17.9 | 16.7 | 15.5 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 22.7 | 21.4 | 20.2 | 19.0 | 17.7 | 16.5 | 15.3 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 22.4 | 21.2 | 20.0 | 18.8 | 17.5 | 16.3 | 15.1 |

Bridge 490054

| Critical Vehicle |  | Section Loss |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 95 | 90 | 85 | 80 | 75 | 70 |
|  | 100 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 46.6 | 44.1 | 41.4 | 38.6 | 35.9 | 33.1 | 30.3 |
|  | 99 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 46.0 | 43.5 | 40.8 | 38.1 | 35.4 | 32.6 | 29.8 |
|  | 98 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 45.3 | 42.9 | 40.2 | 37.5 | 34.8 | 32.0 | 29.3 |
|  | 97 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 44.7 | 42.2 | 39.6 | 36.9 | 34.3 | 31.5 | 28.8 |
|  | 96 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 44.0 | 41.6 | 39.0 | 36.3 | 33.7 | 31.0 | 28.3 |
|  | 95 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 43.4 | 41.0 | 38.4 | 35.8 | 33.1 | 30.5 | 27.8 |
|  | 94 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 42.7 | 40.3 | 37.8 | 35.2 | 32.6 | 29.9 | 27.3 |
|  | 93 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 42.1 | 39.7 | 37.2 | 34.6 | 32.0 | 29.4 | 26.8 |
|  | 92 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 41.4 | 39.1 | 36.6 | 34.0 | 31.5 | 28.9 | 26.3 |
|  | 91 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 40.7 | 38.4 | 35.9 | 33.4 | 30.9 | 28.4 | 25.8 |
|  | 90 | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH | SNSH |
|  |  | 40.1 | 37.8 | 35.3 | 32.9 | 30.4 | 27.8 | 25.3 |

Bridge 590054

## Group 2 Bridges, Rating Vehicles:

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op <br> Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 59 | - | \#N/A | 59 | - | \#N/A | 59 | - | \#N/A |
| 58 | 43.9 | TNAGT5B | 58 | - | \#N/A | 58 | 43.9 | TNAGT5B |
| 57 | 41.3 | SNS7B | 57 | 41.3 | SNS7B | 57 | 42.1 | TNAGT5B |
| 56 | 39.5 | SNS6A | 56 | 39.5 | SNS6A | 56 | 40.4 | TNAGT5B |
| 55 | 37.9 | SNS6A | 55 | 37.9 | SNS6A | 55 | 38.7 | TNAGT5B |
| 54 | 35.5 | SNS5A | 54 | 35.5 | SNS5A | 54 | 37.0 | TNT6A |
| 53 | 33.9 | SNS5A | 53 | 33.9 | SNS5A | 53 | 35.3 | TNT6A |
| 52 | 32.2 | SNS5A | 52 | 32.2 | SNS5A | 52 | 32.9 | TNAGRIT3 |
| 51 | 30.6 | SNS5A | 51 | 30.6 | SNS5A | 51 | 31.2 | TNAGRIT3 |
| 50 | 28.9 | SNS5A | 50 | 28.9 | SNS5A | 50 | 29.6 | TNAGRIT3 |
| 49 | 26.3 | SNCOTTS3 | 49 | 26.3 | SNCOTTS3 | 49 | 27.9 | TNAGRIT3 |

## Bridge 090096

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op <br> Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 67 | - | \#N/A | 67 | - | \#N/A | 67 | - | \#N/A |
| 66 | 44.3 | TNAGT5B | 66 | - | \#N/A | 66 | 44.3 | TNAGT5B |
| 65 | 41.3 | SNS7B | 65 | 41.3 | SNS7B | 65 | 43.1 | TNAGT5B |
| 64 | 40.2 | SNS7B | 64 | 40.2 | SNS7B | 64 | 41.9 | TNAGT5B |
| 63 | 39.0 | SNS6A | 63 | 39.0 | SNS6A | 63 | 40.7 | TNAGT5B |
| 62 | 37.8 | SNS6A | 62 | 37.8 | SNS6A | 62 | 39.6 | TNAGT5B |
| 61 | 35.4 | SNS5A | 61 | 35.4 | SNS5A | 61 | 38.4 | TNAGT5B |
| 60 | 34.3 | SNS5A | 60 | 34.3 | SNS5A | 60 | 37.2 | TNAGT5B |
| 59 | 33.2 | SNS5A | 59 | 33.2 | SNS5A | 59 | 36.0 | TNAGT5B |
| 58 | 32.1 | SNS5A | 58 | 32.1 | SNS5A | 58 | 34.8 | TNAGT5B |
| 57 | 31.0 | SNS5A | 57 | 31.0 | SNS5A | 57 | 32.4 | TNAGRIT3 |
| 56 | 29.9 | SNS5A | 56 | 29.9 | SNS5A | 56 | 31.3 | TNAGRIT3 |
| 55 | 26.8 | SNCOTTS3 | 55 | 26.8 | SNCOTTS3 | 55 | 30.1 | TNAGRIT3 |
| 54 | 25.8 | SNCOTTS3 | 54 | 25.8 | SNCOTTS3 | 54 | 29.0 | TNAGRIT3 |

Bridge 330048

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 81 | - | \#N/A | 81 | - | \#N/A | 81 | - | \#N/A |
| 80 | 41.6 | SNS7B | 80 | 41.6 | SNS7B | 80 | 43.8 | TNAGT5B |
| 79 | 40.6 | SNS7B | 79 | 40.6 | SNS7B | 79 | 42.7 | TNAGT5B |
| 78 | 39.4 | SNS6A | 78 | 39.4 | SNS6A | 78 | 41.6 | TNAGT5B |
| 77 | 38.3 | SNS6A | 77 | 38.3 | SNS6A | 77 | 40.5 | TNAGT5B |
| 76 | 37.3 | SNS6A | 76 | 37.3 | SNS6A | 76 | 39.3 | TNAGT5B |
| 75 | 34.7 | SNS5A | 75 | 34.7 | SNS5A | 75 | 38.2 | TNAGT5B |
| 74 | 33.7 | SNS5A | 74 | 33.7 | SNS5A | 74 | 37.1 | TNAGT5B |
| 73 | 32.6 | SNS5A | 73 | 32.6 | SNS5A | 73 | 35.9 | TNAGT5B |
| 72 | 31.6 | SNS5A | 72 | 31.6 | SNS5A | 72 | 34.8 | TNAGT5B |
| 71 | 30.6 | SNS5A | 71 | 30.6 | SNS5A | 71 | 32.2 | TNAGRIT3 |
| 70 | 27.1 | SNCOTTS3 | 70 | 27.1 | SNCOTTS3 | 70 | 31.1 | TNAGRIT3 |
| 69 | 26.1 | SNCOTTS3 | 69 | 26.1 | SNCOTTS3 | 69 | 30.0 | TNAGRIT3 |

## Bridge 330049

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 59 | - | \#N/A | 59 | - | \#N/A | 59 | - | \#N/A |
| 58 | 44.6 | TNAGT5B | 58 | - | \#N/A | 58 | 44.6 | TNAGT5B |
| 57 | 41.6 | SNS7B | 57 | 41.6 | SNS7B | 57 | 43.2 | TNAGT5B |
| 56 | 40.3 | SNS7B | 56 | 40.3 | SNS7B | 56 | 41.8 | TNAGT5B |
| 55 | 38.9 | SNS6A | 55 | 38.9 | SNS6A | 55 | 40.4 | TNAGT5B |
| 54 | 37.5 | SNS6A | 54 | 37.5 | SNS6A | 54 | 39.1 | TNAGT5B |
| 53 | 35.0 | SNS5A | 53 | 35.0 | SNS5A | 53 | 37.7 | TNAGT5B |
| 52 | 33.8 | SNS5A | 52 | 33.8 | SNS5A | 52 | 36.3 | TNAGT5B |
| 51 | 32.5 | SNS5A | 51 | 32.5 | SNS5A | 51 | 34.9 | TNAGT5B |
| 50 | 31.2 | SNS5A | 50 | 31.2 | SNS5A | 50 | 32.4 | TNAGRIT3 |
| 49 | 29.9 | SNS5A | 49 | 29.9 | SNS5A | 49 | 31.1 | TNAGRIT3 |
| 48 | 26.7 | SNCOTTS3 | 48 | 26.7 | SNCOTTS3 | 48 | 29.7 | TNAGRIT3 |
| 47 | 25.5 | SNCOTTS3 | 47 | 25.5 | SNCOTTS3 | 47 | 28.4 | TNAGRIT3 |

Bridge 330302

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op <br> Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 63 | - | \#N/A | 63 | - | \#N/A | 63 | - | \#N/A |
| 62 | 41.1 | SNS7B | 62 | 41.1 | SNS7B | 62 | 43.6 | TNAGT5B |
| 61 | 39.6 | SNS6A | 61 | 39.6 | SNS6A | 61 | 42.1 | TNAGT5B |
| 60 | 38.2 | SNS6A | 60 | 38.2 | SNS6A | 60 | 40.6 | TNAGT5B |
| 59 | 35.1 | SNS5A | 59 | 35.1 | SNS5A | 59 | 39.1 | TNAGT5B |
| 58 | 33.7 | SNS5A | 58 | 33.7 | SNS5A | 58 | 37.6 | TNAGT5B |
| 57 | 32.4 | SNS5A | 57 | 32.4 | SNS5A | 57 | 36.1 | TNAGT5B |
| 56 | 31.0 | SNS5A | 56 | 31.0 | SNS5A | 56 | 32.9 | TNAGRIT3 |
| 55 | 26.9 | SNCOTTS3 | 55 | 26.9 | SNCOTTS3 | 55 | 31.4 | TNAGRIT3 |
| 54 | 25.7 | SNCOTTS3 | 54 | 25.7 | SNCOTTS3 | 54 | 30.0 | TNAGRIT3 |

## Bridge 330305

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 73 | - | \#N/A | 73 | - | \#N/A | 73 | - | \#N/A |
| 72 | 44.1 | TNAGT5B | 72 | - | \#N/A | 72 | 44.1 | TNAGT5B |
| 71 | 41.4 | SNS7B | 71 | 41.4 | SNS7B | 71 | 43.0 | TNAGT5B |
| 70 | 40.4 | SNS7B | 70 | 40.4 | SNS7B | 70 | 41.9 | TNAGT5B |
| 69 | 39.3 | SNS6A | 69 | 39.3 | SNS6A | 69 | 40.8 | TNAGT5B |
| 68 | 38.2 | SNS6A | 68 | 38.2 | SNS6A | 68 | 39.8 | TNAGT5B |
| 67 | 37.2 | SNS6A | 67 | 37.2 | SNS6A | 67 | 38.7 | TNAGT5B |
| 66 | 35.1 | SNS5A | 66 | 35.1 | SNS5A | 66 | 37.6 | TNAGT5B |
| 65 | 34.0 | SNS5A | 65 | 34.0 | SNS5A | 65 | 36.5 | TNAGT5B |
| 64 | 33.0 | SNS5A | 64 | 33.0 | SNS5A | 64 | 35.4 | TNAGT5B |
| 63 | 32.0 | SNS5A | 63 | 32.0 | SNS5A | 63 | 34.4 | TNAGT5B |
| 62 | 31.0 | SNS5A | 62 | 31.0 | SNS5A | 62 | 32.2 | TNAGRIT3 |
| 61 | 30.0 | SNS5A | 61 | 30.0 | SNS5A | 61 | 31.2 | TNAGRIT3 |
| 60 | 27.1 | SNCOTTS3 | 60 | 27.1 | SNCOTTS3 | 60 | 30.1 | TNAGRIT3 |
| 59 | 26.2 | SNCOTTS3 | 59 | 26.2 | SNCOTTS3 | 59 | 29.1 | TNAGRIT3 |

## Bridge 500062

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 100 | 34.6 | SNS5A | 100 | 34.6 | SNS5A | 100 | 36.1 | TNT6A |
| 99 | 33.8 | SNS5A | 99 | 33.8 | SNS5A | 99 | 35.3 | TNAGT5B |
| 98 | 33.1 | SNS5A | 98 | 33.1 | SNS5A | 98 | 34.5 | TNAGT5B |
| 97 | 32.4 | SNAGGRS4 | 97 | 32.4 | SNAGGRS4 | 97 | 33.7 | TNAGT5B |
| 96 | 31.6 | SNS5A | 96 | 31.6 | SNS5A | 96 | 32.4 | TNAGRIT3 |
| 95 | 30.9 | SNS5A | 95 | 30.9 | SNS5A | 95 | 31.6 | TNAGRIT3 |
| 94 | 30.1 | SNS5A | 94 | 30.1 | SNS5A | 94 | 30.8 | TNAGRIT3 |
| 93 | 29.4 | SNS5A | 93 | 29.4 | SNS5A | 93 | 30.1 | TNAGRIT3 |
| 92 | 28.6 | SNS5A | 92 | 28.6 | SNS5A | 92 | 29.3 | TNAGRIT3 |
| 91 | 26.8 | SNCOTTS3 | 91 | 26.8 | SNCOTTS3 | 91 | 28.6 | TNAGRIT3 |
| 90 | 26.1 | SNCOTTS3 | 90 | 26.1 | SNCOTTS3 | 90 | 27.8 | TNAGRIT3 |

## Bridge 590126

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 66 | - | \#N/A | 66 | - | \#N/A | 66 | - | \#N/A |
| 65 | 43.4 | TNAGT5B | 65 | - | \#N/A | 65 | 43.4 | TNAGT5B |
| 64 | 41.3 | SNS7B | 64 | 41.3 | SNS7B | 64 | 41.8 | TNAGT5B |
| 63 | 39.1 | SNS6A | 63 | 39.1 | SNS6A | 63 | 40.2 | TNAGT5B |
| 62 | 37.5 | SNS6A | 62 | 37.5 | SNS6A | 62 | 38.6 | TNAGT5B |
| 61 | 35.3 | SNS5A | 61 | 35.3 | SNS5A | 61 | 36.9 | TNAGT5B |
| 60 | 33.8 | SNS5A | 60 | 33.8 | SNS5A | 60 | 35.3 | TNAGT5B |
| 59 | 32.2 | SNS5A | 59 | 32.2 | SNS5A | 59 | 32.8 | TNT4A |
| 58 | 30.7 | SNS5A | 58 | 30.7 | SNS5A | 58 | 31.2 | TNT4A |
| 57 | 29.1 | SNS5A | 57 | 29.1 | SNS5A | 57 | 29.6 | TNT4A |
| 56 | 26.2 | SNCOTTS3 | 56 | 26.2 | SNCOTTS3 | 56 | 28.1 | TNT4A |

Bridge 590169

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 59 | - | \#N/A | 59 | - | \#N/A | 59 | - | \#N/A |
| 58 | 42.6 | TNAGT5B | 58 | - | \#N/A | 58 | 42.6 | TNAGT5B |
| 57 | 39.5 | SNS6A | 57 | 39.5 | SNS6A | 57 | 40.0 | TNAGT5B |
| 56 | 36.9 | SNS6A | 56 | 36.9 | SNS6A | 56 | 37.4 | TNAGRIT4 |
| 55 | 33.9 | SNAGGRS4 | 55 | 33.9 | SNAGGRS4 | 55 | 34.7 | TNAGT5B |
| 54 | 31.3 | SNAGGRS4 | 54 | 31.3 | SNAGGRS4 | 54 | 31.6 | TNT4A |
| 53 | 28.8 | SNAGGRS4 | 53 | 28.8 | SNAGGRS4 | 53 | 29.0 | TNT4A |
| 52 | 25.4 | SNCOTTS3 | 52 | 25.4 | SNCOTTS3 | 52 | 26.4 | TNT4A |
| 51 | 22.9 | SNCOTTS3 | 51 | 22.9 | SNCOTTS3 | 51 | 23.8 | TNT4A |

## Bridge 590182

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 67 | - | \#N/A | 67 | - | \#N/A | 67 | - | \#N/A |
| 66 | 44.3 | TNAGT5B | 66 | - | \#N/A | 66 | 44.3 | TNAGT5B |
| 65 | 41.6 | SNS7B | 65 | 41.6 | SNS7B | 65 | 42.8 | TNAGT5B |
| 64 | 40.2 | SNS7B | 64 | 40.2 | SNS7B | 64 | 41.4 | TNAGT5B |
| 63 | 38.8 | SNS6A | 63 | 38.8 | SNS6A | 63 | 40.0 | TNAGT5B |
| 62 | 37.4 | SNS6A | 62 | 37.4 | SNS6A | 62 | 38.5 | TNAGT5B |
| 61 | 35.2 | SNS5A | 61 | 35.2 | SNS5A | 61 | 37.1 | TNAGT5B |
| 60 | 33.8 | SNS5A | 60 | 33.8 | SNS5A | 60 | 35.6 | TNAGT5B |
| 59 | 32.4 | SNS5A | 59 | 32.4 | SNS5A | 59 | 34.2 | TNAGT5B |
| 58 | 31.1 | SNS5A | 58 | 31.1 | SNS5A | 58 | 32.0 | TNAGRIT3 |
| 57 | 29.7 | SNS5A | 57 | 29.7 | SNS5A | 57 | 30.6 | TNAGRIT3 |
| 56 | 27.0 | SNCOTTS3 | 56 | 27.0 | SNCOTTS3 | 56 | 29.2 | TNAGRIT3 |
| 55 | 25.7 | SNCOTTS3 | 55 | 25.7 | SNCOTTS3 | 55 | 27.7 | TNAGRIT3 |

Bridge 590404

| All Vehicles |  |  |
| :---: | :---: | :---: |
| $\%$ eff | Min Op <br> Wt | Control RV |
| 55 | - | \#N/A |
| 54 | 44.7 | TNAGT5B |
| 53 | 41.7 | SNS7B |
| 52 | 39.7 | SNS6A |
| 51 | 37.7 | SNS6A |
| 50 | 35.1 | SNS5A |
| 49 | 33.1 | SNS5A |
| 48 | 31.1 | SNS5A |
| 47 | 29.1 | SNS5A |
| 46 | 26.2 | SNCOTTS3 |


| Single Unit Vehicles |  |  |
| :---: | :---: | :---: |
| eff | Min Op Wt | Control RV |
|  | - | \#N/A |
| 54 | - | \#N/A |
| 53 | 41.7 | SNS7B |
| 52 | 39.7 | SNS6A |
| 51 | 37.7 | SNS6A |
| 50 | 35.1 | SNS5A |
| 49 | 33.1 | SNS5A |
| 48 | 31.1 | SNS5A |
| 47 | 29.1 | SNS5A |
| 46 | 26.2 | SNCOTTS3 |


| Tandem Trucks |  |  |
| :---: | :---: | :---: |
| \% eff | Min Op Wt | Control RV |
| 55 | - | \#N/A |
| 54 | 44.7 | TNAGT5B |
| 53 | 42.6 | TNAGT5B |
| 52 | 40.6 | TNT6A |
| 51 | 38.5 | TNAGT5B |
| 50 | 36.5 | TNT6A |
| 49 | 34.4 | TNT6A |
| 48 | 31.8 | TNAGRIT3 |
| 47 | 29.7 | TNAGRIT3 |
| 44 | 27.7 | TNAGRIT3 |

## Bridge 590516

| All Vehicles |  |  | Single Unit Vehicles |  |  | Tandem Trucks |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV | \% eff | Min Op Wt | Control RV |
| 74 | - | \#N/A | 74 | - | \#N/A | 74 | - | \#N/A |
| 73 | 44.5 | TNAGT5B | 73 | - | \#N/A | 73 | 44.5 | TNAGT5B |
| 72 | 43.9 | TNAGT5B | 72 | - | \#N/A | 72 | 43.9 | TNAGT5B |
| 71 | 41.8 | SNS7B | 71 | 41.8 | SNS7B | 71 | 43.3 | TNAGT5B |
| 70 | 41.2 | SNS7B | 70 | 41.2 | SNS7B | 70 | 42.6 | TNAGT5B |
| 69 | 40.7 | SNS7B | 69 | 40.7 | SNS7B | 69 | 42.0 | TNAGT5B |
| 68 | 40.1 | SNS7B | 68 | 40.1 | SNS7B | 68 | 41.4 | TNAGT5B |
| 67 | 39.4 | SNS6A | 67 | 39.4 | SNS6A | 67 | 40.8 | TNAGT5B |
| 66 | 38.8 | SNS6A | 66 | 38.8 | SNS6A | 66 | 40.2 | TNAGT5B |
| 65 | 38.2 | SNS6A | 65 | 38.2 | SNS6A | 65 | 39.6 | TNAGT5B |
| 64 | 37.6 | SNS6A | 64 | 37.6 | SNS6A | 64 | 39.0 | TNAGT5B |
| 63 | 37.0 | SNS6A | 63 | 37.0 | SNS6A | 63 | 38.4 | TNAGT5B |
| 62 | 35.4 | SNS5A | 62 | 35.4 | SNS5A | 62 | 37.8 | TNAGT5B |
| 61 | 34.9 | SNS5A | 61 | 34.9 | SNS5A | 61 | 37.2 | TNAGT5B |
| 60 | 34.3 | SNS5A | 60 | 34.3 | SNS5A | 60 | 36.6 | TNAGT5B |
| 59 | 33.7 | SNS5A | 59 | 33.7 | SNS5A | 59 | 35.9 | TNAGT5B |
| 58 | 33.1 | SNS5A | 58 | 33.1 | SNS5A | 58 | 35.3 | TNAGT5B |
| 57 | 32.6 | SNS5A | 57 | 32.6 | SNS5A | 57 | 34.7 | TNAGT5B |
| 56 | 32.0 | SNS5A | 56 | 32.0 | SNS5A | 56 | 34.1 | TNAGT5B |
| 55 | 31.4 | SNS5A | 55 | 31.4 | SNS5A | 55 | 32.6 | TNAGRIT3 |
| 54 | 30.9 | SNAGGRS4 | 54 | 30.9 | SNAGGRS4 | 54 | 32.0 | TNAGRIT3 |
| 53 | 30.3 | SNS5A | 53 | 30.3 | SNS5A | 53 | 31.4 | TNAGRIT3 |
| 52 | 29.7 | SNS5A | 52 | 29.7 | SNS5A | 52 | 30.8 | TNAGRIT3 |
| 51 | 29.1 | SNS5A | 51 | 29.1 | SNS5A | 51 | 30.2 | TNAGRIT3 |
| 50 | 26.8 | SNCOTTS3 | 50 | 26.8 | SNCOTTS3 | 50 | 29.6 | TNAGRIT3 |

Bridge 840010

Appendix II:
Truck Generation Program Instruction Manual

## Introduction

The computer program performs two essentially independent tasks:

1. It generates possible truck configurations for numerous axle combinations with varying lengths between the axles as allowed by the North Carolina Statutory Weights of Legal Vehicles (as outlined in the NC general statute § 20-118 (b)(3)). The program also has the option of generating trucks according to the Federal Bridge Formula (FBF). For each generated truck, the program calculates the maximum moment produced by each truck for a specified bridge span.
2. It calculates the maximum moment corresponding to the specified bridge span for any number of specified vehicle configurations.

## Input Files

The program reads the following input files:

1. Main input file: "ncst_in.txt". This file contains all the parameters desired for the program output, like which number of axles to include, whether to use the NC statute of the federal bridge formula, the distances between axles, and the specified bridge span, among other information. A sample main input file is shown in Figure 1.
```
Input file for Automatic Truck Generation of North Carolina Legal Vehicles (According to Statute 20-118 (b) 3.)
Truck Reports: # of axles followed by 1 (print report) or 0 (do not print). Leave space between numbers.
Single Vehicles
2 1
31
4 1
7 5 1
8 6 1
Tractor Trailers
3 1
41
51
60
Determination of Maximum Legal Weight: 1 = NC statute (NCS); 0 = Federal Bridge Formula (FBF)
1
Number of Axle Combinations flag: 1 = reduced; 2 = intermediate; 3 = large. Default: reduced.
1
Maximum Weight Exception and truck length for exception to take effect.
90000.0 9999.0
Specified distances between axles - SINGLE VEHICLE 2-axles
Number of distances
4
Actual distances
4.0 9.0 11.0 14.0
Specified distances between axles - SINGLE VEHICLE 3-axles
Number of distances
4
Actual distances
4.0 9.0 11.0 14.0
.
Actual distances
4.0 9.0 11.0 14.0
Specified distances between axles - TRACTOR TRAILER 3-axles
number of distances
4
Actual distances
4.0 9.0 11.0 14.0
Specified distances between axles - TRACTOR TRAILER 4-axles
number of distances
4
Actual distances
4.0 9.0 11.0 14.0
i
Span for moment calculations
100.0
EOF
```

Figure 1. Sample Main Input File ("ncst_in.txt").
2. NC statute file: "statute_weights.txt". This file contains the NC statute weights and distances between axles in the form of a matrix. A sample NC statute file is shown in Figure 2.


Figure 2. NC statute weights and NC statute file ("statute_weights.txt").
3. Specified Vehicles file: "specified_vehicles.txt". This file contains any number of specified vehicles according to a specific format that is explained below. A sample specified vehicles file is shown in Figure 3.

```
NCDOT SPECIFIED VEHICLES LIST
What follows are }6\mathrm{ records with the number of axles followed by the number of
records per number of axles
27
36
47
56
65
74
TWO-AXLE VEHICLES
7
SNSH 2 14 -1 27000 5000 14 22000
SNGARBS2 2 14 -1 40000 23500 14 16500
SNAGRIS2 2 14 -1 44000 22000 14 22000
F_LN7000 2 22 -1 26000 7000 22 19000
FORDE350 2 16 -1 12000 4200 16 7800
HINO_268 2 26 -1 29000 10000 26 19000
THREE-AXLE VEHICLES
6
SNCOTTS3 3 15 -1 54500 4500 11 25000 4 25000
TNAGRIT3 3 18 -1 66000 22000 9}22000 9 22000
SPI112FT 3 25 -1 82000 24000 21 29000 4 29000
SAI75FT 3 26 -1 76000 24000 22 26000 4 26000
SP95FT 3 21 -1 63000 23000 17 20000 4 20000
3AX_CONC 3 13 -1 66000 20000 9 23000 4 23000
FOUR-AXLE VEHICLES
7
SNAGGRS4 4 17 -1 69850 16000 9
TNT4A 4 22 -1 66150 12100 9 12050 9 21000 4 21000
TNAGRIT4 4 22 -1 86000 22000 9 22000 9 21000 4 21000
FD4000 4 17 -1 90000 21000 9 23000 4 23000 4 23000
4AX_CONC 4 17 -1 66000 20000 9
WP53+IP4 4 58 -1 82000}14000 19 23000 35 22500 4 2250
SC40+IP4 4 52 -1 87000 14000 19 23000 29 25000 4 25000
FIVE-AXLE VEHICLES
6
SNS5A 5 5 21 -1 [1100 12100 9
TNAGT5A 5 26 -1 90000 22000 9 21000 4 21000 9
TNAGT5B 5 26 -1 90000 6000 9 21000 4 21000 9 21000 4 21000
WP53+IP6 5 60 -1 105000 14000 17 23000 4 23000 35 22500 4 22500
SC40+IP6 5 52 -1 102000 12000 15 20000 4 20000 29 25000 & 25000
FD5000 5 21 -1 113000 21000 9 23000 4 23000 4 23000 4 23000
```

Figure 3. Specified Vehicles file ("specified_vehicles.txt").

## Main Input File Contents

The main input file ("ncst_in.txt") can be thought of as comprising six different sections. They are as follows.

Section 1. This section has two columns. The left column corresponds to the number of axles on the truck, and the right column is a Boolean operator for that truck type. If a number of axles combination has a value of 1 in front of it (i.e. in the second column), the truck type (i.e. trucks with this number of axles) will be generated and included in the output file; if the axle combination has a value of 0 (zero), trucks with that number of axles will not be generated and hence will not be included in the output file. Running the program with an input file like the one shown in Figure 1 for instance, will return results for single vehicles with 2 to 7 axles, and tractor trailer trucks with 3 to 5 axles.

Section 2. This section allows the user to specify a parameter that will determine the way the program calculates maximum legal weight for each generated truck. If this parameter is equal to 1 , the program uses the NC statute. If it is equal to 0 , the program uses the federal bridge formula. Default is the NC statute.

Section 3. The program can generate a range of axle combinations for each truck axle type. This is controlled with a single parameter in this section. If this parameter is equal to 1 a small number of axle combinations (termed "reduced") will be generated. If this parameter is equal to 2 , and intermediate number of axle combinations will be generated, and if it is equal to 3 , a large number of axle combinations will be generated. The number of trucks to be generated also depends on the number of axles, and on whether the truck is a single vehicle or a tractor trailer.

In its present form, the number of trucks generated by the program for each number of axles, ranges from 3 (for single-vehicle 2-axle configurations) to 1128 (for 7-axle tractor trailers with the large axle combination option).

Section 4. This section allows the user to specify a maximum truck weight corresponding to an exception (e.g., a weight that is not in the statute matrix) and a minimum truck length to apply the exception. For the values specified in this section of Figure 1, for instance, the exception weight is $90,000 \mathrm{lb}$. and this weight is to be applied to trucks with a minimum length of $9,999 \mathrm{ft}$. (which effectively prevents the exception to be applied). If this second number were equal to say 34 , the program will apply the exception to all trucks with lengths equal to or larger than 34 ft .

Section 5. This section allows the user to enter the truck axle spacings that will be used to generate the truck configurations. In its present form the program requires the input of four different distances in ascending order for each axle configuration (these distances are labeled: a, b, c, and d). Distances are assumed in feet. Distance a, is assumed to be the distance corresponding to a tandem axle. A different set of distances can be specified for each axle configuration. These values can be changed by the user; however, it is important that the values are entered in ascending order, and that the smallest distance value corresponds to the distance between the axles in a tandem axle. Also, only permutations of distances $b, c$, and $d$ are considered when generating the axle combinations. A schematic representation of these ideas is shown in Figure 4.


Figure 4: Truck Axle Spacing Diagram with a/b/c Distances.

Section 6. The sixth and final section allows the user to specify a span (in feet) for the maximum bending moment calculations.

## Specified Vehicles File ("specified_vehicles.txt")

This file has two sections. Section 1 contains the number of vehicles for each axle configuration. The values shown in Figure 3 for instance, mean that the file will contain 7 2-axle vehicles, 6 3- axle vehicles, 7 4-axle vehicles, etc. Section 2 contains the actual specified vehicles in the following format:

Field 1 contains the truck name with no more than 6 characters.

Field 2 contains the number of axles.

Field 3 contains the total length of the truck in feet.

Field 4 contains the NC statute weight of the truck (currently not used).

Field 5 contains the actual weight of the truck.

Field 6 to Field $2 * n \_$axles +3 contain the combination axle weight and distance to the next axle (where $n \_$axles is the number of axles of the truck).

Field $2 * n \_$axles +4 contains the weight of the last axle of the truck.

## Notes:

1. All title (or comment) lines in all files are read by the program but their contents are ignored. For instance, in the main input file the contents of the first three lines are ignored by the program. These lines are in the files to remind the user of the subsequent content of the file. The contents of these lines can be modified but the lines themselves must not be removed.
2. Some lines in the input files contain the number of records that follow the line. For instance, in the specified vehicles file (see Figure 3), the line that follows the comment line "TWO-AXLE VEHICLES" contains a 7. This means that there are 7 records of 2-axle vehicles that follow that line. These numbers must correspond exactly to the number of records that follow the line and to the numbers in Section 1 of the file (see above).

## Output Files

The program output consists of three (3) files: "Trucks_out.txt," "WARNINGS_out.txt," and "DEBUG_out.txt." The contents of these files are described next.
"Trucks_out.txt": This is the main output file of the program. This file has to sections. Section 1 contains the output corresponding to the specified vehicles that were read from the "specified_vehicles,txt" file by the program. Section 2 contains the generated (possible) truck configurations. The output format for this file follows closely the format described above for the specified vehicles file. A sample output file is shown in Figure 5

The format of the main output file is as follows:

Field 1 contains the truck name with maximum of 6 characters for the specified trucks and a consecutive number for the generated trucks.

Field 2 contains the number of axles.

Field 3 contains the total length of the truck in feet.

Field 4 contains the NC statute weight of the truck (currently not used).

Field 5 contains the actual weight of the truck.

Field 6 to Field 2*n_axles +3 contain the combination axle weight and distance to the next axle (where $n \_a x l e s$ is the number of axles of the truck).

Field $2 * n \_$axles +4 contains the weight of the last axle of the truck.

Field $2 *$ n_axles +5 contains the span specified for the bending moment calculations, and Field $2 *$ n_axles +6 contains the maximum bending moment for the specified span.
"WARNINGS_out.txt": This file contains warnings and errors. A common warning is generated when there is a truck-length-number-of-axles combination that is
not in the NC statute (the statute weights matrix contains a -1 in this position, see Figure 2). In this case the program determines the weight of the truck using the Federal Bridge Formula and issues the corresponding warning. In general, warnings are normal, but errors are not, and the output of the program must not be trusted when errors occur.
"DEBUG_out.txt": This file contains debug information that can be ignored by the user. It is there to help developers pinpoint problems with the code.

## Appendix III: <br> Sample Truck Generation Program Output File

    SINGLE VEHICLE 2-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:
    | Trck | Axls | Lngth | NCS | Weight Ax1 | d1 | Ax2 | Span | Mmax |  |
| :---: | :---: | ---: | ---: | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | 2 | 14 | 44000 | 44000 | 22000 | 14 | 22000 | 100 | 946 |
| 2 | 2 | 11 | 41000 | 41000 | 20500 | 11 | 20500 | 100 | 912 |
| 3 | 2 | 9 | 38000 | 38000 | 19000 | 9 | 19000 | 100 | 864 |

SINGLE VEHICLE 3-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:

Trck Axls Lngth NCS Weight Ax1 d1 Ax2 d2 Ax3 Span Mmax
$\begin{array}{llllllllllll}1 & 3 & 18 & 49500 & 49500 & 18500 & 14 & 15500 & 4 & 15500 & 100 & 1077\end{array}$
$\begin{array}{llllllllllll}2 & 3 & 15 & 47000 & 47000 & 17667 & 11 & 14667 & 4 & 14667 & 100 & 1049\end{array}$
$\begin{array}{llllllllllll}3 & 3 & 13 & 45500 & 45500 & 17167 & 9 & 14167 & 4 & 14167 & 100 & 1032\end{array}$

SINGLE VEHICLE 4-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:

| Trck | Axls | Lngth NCS | Weight Ax1 | d1 | Ax2 | d2 | Ax3 | d3 | Ax4 | Span Mmax |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4 | 22 | 56500 | 56500 | 21125 | 14 | 11792 | 4 | 11792 | 4 | 11792 | 100 | 1194 |
| 2 | 4 | 19 | 54500 | 54500 | 20625 | 11 | 11292 | 4 | 11292 | 4 | 11292 | 100 | 1181 |
| 3 | 4 | 17 | 53500 | 53500 | 20375 | 9 | 11042 | 4 | 11042 | 4 | 11042 | 100 | 1180 |

SINGLE VEHICLE 5-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:

| Trck | Axls | Lngth $N C S$ | Weight Ax1 | d1 | Ax2 | d2 | Ax3 | d3 | Ax4 | d4 | Ax5 | Span Mmax |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 5 | 31 | 67500 | 67500 | 15900 | 14 | 12900 | 4 | 12900 | 9 | 12900 | 4 | 12900 | 100 | 1377 |
| 2 | 5 | 33 | 68500 | 68500 | 16100 | 14 | 13100 | 4 | 13100 | 11 | 13100 | 4 | 13100 | 100 | 1371 |
| 3 | 5 | 36 | 70500 | 70500 | 16500 | 14 | 13500 | 4 | 13500 | 14 | 13500 | 4 | 13500 | 100 | 1371 |
| 4 | 5 | 28 | 65500 | 65500 | 15500 | 11 | 12500 | 4 | 12500 | 9 | 12500 | 4 | 12500 | 100 | 1359 |
| 5 | 5 | 33 | 68500 | 68500 | 16100 | 11 | 13100 | 4 | 13100 | 14 | 13100 | 4 | 13100 | 100 | 1356 |
| 6 | 5 | 30 | 66500 | 66500 | 15700 | 11 | 12700 | 4 | 12700 | 11 | 12700 | 4 | 12700 | 100 | 1354 |
| 7 | 5 | 31 | 67500 | 67500 | 15900 | 9 | 12900 | 4 | 12900 | 14 | 12900 | 4 | 12900 | 100 | 1352 |
| 8 | 5 | 28 | 65500 | 65500 | 15500 | 9 | 12500 | 4 | 12500 | 11 | 12500 | 4 | 12500 | 100 | 1349 |
| 9 | 5 | 26 | 64000 | 64000 | 15200 | 9 | 12200 | 4 | 12200 | 9 | 12200 | 4 | 12200 | 100 | 1343 |
| 10 | 5 | 26 | 64000 | 64000 | 20400 | 14 | 10900 | 4 | 10900 | 4 | 10900 | 4 | 10900 | 100 | 1329 |
| 11 | 5 | 23 | 62500 | 62500 | 20100 | 11 | 10600 | 4 | 10600 | 4 | 10600 | 4 | 10600 | 100 | 1327 |
| 12 | 5 | 21 | 61000 | 61000 | 19800 | 9 | 10300 | 4 | 10300 | 4 | 10300 | 4 | 10300 | 100 | 1314 |

SINGLE VEHICLE 6-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:

| Trck | Axls | Lngth | NCS | Weight | Ax1 | d1 | Ax2 | d2 | Ax3 | d3 | Ax4 | d4 | Ax5 | d5 | Ax6 | Span | Mmax |
| :---: | :---: | :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 1 | 6 | 40 | 78000 | 78000 | 19333 | 14 | 9833 | 4 | 9833 | 4 | 9833 | 4 | 9833 | 14 | 19333 | 100 | 1485 |
| 2 | 6 | 37 | 76000 | 76000 | 19000 | 11 | 9500 | 4 | 9500 | 4 | 9500 | 4 | 9500 | 14 | 19000 | 100 | 1472 |
| 3 | 6 | 37 | 76000 | 76000 | 19000 | 14 | 9500 | 4 | 9500 | 4 | 9500 | 4 | 9500 | 11 | 19000 | 100 | 1472 |
| 4 | 6 | 35 | 75000 | 75000 | 18833 | 9 | 9333 | 4 | 9333 | 4 | 9333 | 4 | 9333 | 14 | 18833 | 100 | 1471 |
| 5 | 6 | 35 | 75000 | 75000 | 18833 | 14 | 9333 | 4 | 9333 | 4 | 9333 | 4 | 9333 | 9 | 18833 | 100 | 1471 |
| 6 | 6 | 30 | 72000 | 72000 | 20667 | 14 | 10267 | 4 | 10267 | 4 | 10267 | 4 | 10267 | 4 | 10267 | 100 | 1470 |
| 7 | 6 | 34 | 74500 | 74500 | 18750 | 11 | 9250 | 4 | 9250 | 4 | 9250 | 4 | 9250 | 11 | 18750 | 100 | 1470 |
| 8 | 6 | 27 | 70000 | 70000 | 20333 | 11 | 9933 | 4 | 9933 | 4 | 9933 | 4 | 9933 | 4 | 9933 | 100 | 1458 |
| 9 | 6 | 25 | 69000 | 69000 | 20167 | 9 | 9767 | 4 | 9767 | 4 | 9767 | 4 | 9767 | 4 | 9767 | 100 | 1457 |
| 10 | 6 | 32 | 73000 | 73000 | 18500 | 9 | 9000 | 4 | 9000 | 4 | 9000 | 4 | 9000 | 11 | 18500 | 100 | 1457 |
| 11 | 6 | 32 | 73000 | 73000 | 18500 | 11 | 9000 | 4 | 9000 | 4 | 9000 | 4 | 9000 | 9 | 18500 | 100 | 1457 |
| 12 | 6 | 30 | 72000 | 72000 | 18333 | 9 | 8833 | 4 | 8833 | 4 | 8833 | 4 | 8833 | 9 | 18333 | 100 | 1454 |

SINGLE VEHICLE 7-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:

|  | Axls | Ln | S | Weig | 1 | d1 | Ax2 | d2 | 3 | d3 | Ax4 | d4 | 5 | d5 | A | d6 | Ax7 | Spa | ax |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 7 | 34 | 80000 | 80000 | 20857 | 14 | 9857 | 4 | 9857 | 4 | 9857 | 4 | 9857 | 4 | 9857 | 4 | 9857 | 100 | 1593 |
| 2 | 7 | 31 | 78000 | 78000 | 20571 | 11 | 9571 | 4 | 9571 | 4 | 9571 | 4 | 9571 | 4 | 9571 | 4 | 9571 | 100 | 1582 |
| 3 | 7 | 29 | 77000 | 77000 | 20429 | 9 | 9429 | 4 | 9429 | 4 | 9429 | 4 | 9429 | 4 | 9429 | 4 | 9429 | 100 | 1582 |
| 4 | 7 | 34 | 80000 | 80000 | 1885 | 9 | 845 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 9 | 18857 | 100 | 1578 |
| 5 | 7 | 36 | 80000 | 80000 | 18857 | 9 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 11 | 18857 | 100 | 1559 |
| 6 | 7 | 36 | 80000 | 80000 | 18857 | 11 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 9 | 8857 | 100 | 1559 |
| 7 | 7 | 38 | 80000 | 80000 | 1885 | 11 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 11 | 18857 | 100 | 1540 |
| 8 | 7 | 39 | 80000 | 80000 | 18857 | 9 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 14 | 18857 | 100 | 1531 |
| 9 | 7 | 39 | 80000 | 80000 | 18857 | 14 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 9 | 18857 | 100 | 1531 |
| 10 | 7 | 41 | 80000 | 80000 | 18857 | 11 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 14 | 18857 | 100 | 1512 |
| 11 | 7 | 41 | 80000 | 80000 | 18857 | 14 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 11 | 18857 | 100 | 1512 |
| 12 | 7 | 44 | 80000 | 80000 | 18857 | 14 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 4 | 8457 | 14 | 18857 | 100 | 1484 |

TRACTOR TRAILER 3-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:

| Trck | Axls | Lngth | NCS |  | Weight Ax1 | d1 | Ax2 | d2 | Ax3 |  | Span |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 3 | 28 | 57000 | 57000 | 19000 | 14 | 1900 | 14 | 19000 | 100 | 1159 |
| 2 | 3 | 25 | 54500 | 54500 | 18167 | 11 | 18167 | 14 | 18167 | 100 | 1135 |
| 3 | 3 | 25 | 54500 | 54500 | 18167 | 14 | 18167 | 11 | 18167 | 100 | 1135 |
| 4 | 3 | 23 | 53000 | 53000 | 17667 | 14 | 17667 | 9 | 17667 | 100 | 1122 |
| 5 | 3 | 23 | 53000 | 53000 | 17667 | 9 | 17667 | 14 | 17667 | 100 | 1122 |
| 6 | 3 | 22 | 52500 | 52500 | 17500 | 11 | 17500 | 11 | 17500 | 100 | 1120 |
| 7 | 3 | 20 | 51000 | 51000 | 17000 | 11 | 17000 | 9 | 17000 | 100 | 1105 |
| 8 | 3 | 20 | 51000 | 51000 | 17000 | 9 | 17000 | 11 | 17000 | 100 | 1105 |
| 9 | 3 | 18 | 49500 | 49500 | 16500 | 9 | 16500 | 9 | 16500 | 100 | 1089 |

TRACTOR TRAILER 4-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:

| Trck | Axls | Lngth | NCS | Weight | Ax1 | d1 | Ax2 | d2 | Ax3 | d3 | Ax4 | Span | Mmax |
| :---: | :---: | :---: | ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4 | 32 | 63500 | 63500 | 17375 | 14 | 14375 | 4 | 14375 | 14 | 17375 | 100 | 1281 |
| 2 | 4 | 29 | 61500 | 61500 | 16875 | 11 | 13875 | 4 | 13875 | 14 | 16875 | 100 | 1265 |
| 3 | 4 | 29 | 61500 | 61500 | 16875 | 14 | 13875 | 4 | 13875 | 11 | 16875 | 100 | 1265 |
| 4 | 4 | 27 | 60000 | 60000 | 16500 | 14 | 13500 | 4 | 13500 | 9 | 16500 | 100 | 1250 |
| 5 | 4 | 27 | 60000 | 60000 | 16500 | 9 | 13500 | 4 | 13500 | 14 | 16500 | 100 | 1250 |
| 6 | 4 | 26 | 59500 | 59500 | 16375 | 11 | 13375 | 4 | 13375 | 11 | 16375 | 100 | 1248 |
| 7 | 4 | 29 | 61500 | 61500 | 16875 | 14 | 16875 | 11 | 13875 | 4 | 13875 | 100 | 1239 |
| 8 | 4 | 27 | 60000 | 60000 | 16500 | 14 | 16500 | 9 | 13500 | 4 | 13500 | 100 | 1236 |
| 9 | 4 | 32 | 63500 | 63500 | 17375 | 14 | 17375 | 14 | 14375 | 4 | 14375 | 100 | 1236 |
| 10 | 4 | 24 | 58000 | 58000 | 16000 | 9 | 13000 | 4 | 13000 | 11 | 16000 | 100 | 1232 |
| 11 | 4 | 24 | 58000 | 58000 | 16000 | 11 | 13000 | 4 | 13000 | 9 | 16000 | 100 | 1232 |
| 12 | 4 | 26 | 59500 | 59500 | 16375 | 11 | 16375 | 11 | 13375 | 4 | 13375 | 100 | 1224 |
| 13 | 4 | 29 | 61500 | 61500 | 16875 | 11 | 16875 | 14 | 13875 | 4 | 13875 | 100 | 1223 |
| 14 | 4 | 24 | 58000 | 58000 | 16000 | 11 | 16000 | 9 | 13000 | 4 | 13000 | 100 | 1219 |
| 15 | 4 | 22 | 56500 | 56500 | 15625 | 9 | 12625 | 4 | 12625 | 9 | 15625 | 100 | 1215 |
| 16 | 4 | 27 | 60000 | 60000 | 16500 | 9 | 16500 | 14 | 13500 | 4 | 13500 | 100 | 1210 |
| 17 | 4 | 24 | 58000 | 58000 | 16000 | 9 | 16000 | 11 | 13000 | 4 | 13000 | 100 | 1209 |
| 18 | 4 | 22 | 56500 | 56500 | 15625 | 9 | 15625 | 9 | 12625 | 4 | 12625 | 100 | 1203 |

TRACTOR TRAILER 5-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:

| Trck | Axls | Lngth | NCS | Weight | Ax1 | d1 | Ax2 | d2 | Ax3 | d3 | Ax4 | d4 | Ax5 | Span | Mmax |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 5 | 31 | 67500 | 67500 | 15900 | 14 | 12900 | 4 | 12900 | 9 | 12900 | 4 | 12900 | 100 | 1377 |
| 2 | 5 | 33 | 68500 | 68500 | 16100 | 14 | 13100 | 4 | 13100 | 11 | 13100 | 4 | 13100 | 100 | 1371 |
| 3 | 5 | 36 | 70500 | 70500 | 16500 | 14 | 13500 | 4 | 13500 | 14 | 13500 | 4 | 13500 | 100 | 1371 |
| 4 | 5 | 28 | 65500 | 65500 | 15500 | 11 | 12500 | 4 | 12500 | 9 | 12500 | 4 | 12500 | 100 | 1359 |
| 5 | 5 | 33 | 68500 | 68500 | 16100 | 11 | 13100 | 4 | 13100 | 14 | 13100 | 4 | 13100 | 100 | 1356 |
| 6 | 5 | 30 | 66500 | 66500 | 15700 | 11 | 12700 | 4 | 12700 | 11 | 12700 | 4 | 12700 | 100 | 1354 |
| 7 | 5 | 31 | 67500 | 67500 | 15900 | 9 | 12900 | 4 | 12900 | 14 | 12900 | 4 | 12900 | 100 | 1352 |
| 8 | 5 | 28 | 65500 | 65500 | 15500 | 9 | 12500 | 4 | 12500 | 11 | 12500 | 4 | 12500 | 100 | 1349 |
| 9 | 5 | 26 | 64000 | 64000 | 15200 | 9 | 12200 | 4 | 12200 | 9 | 12200 | 4 | 12200 | 100 | 1343 |
| 10 | 5 | 31 | 67500 | 67500 | 19100 | 14 | 19100 | 9 | 9767 | 4 | 9767 | 4 | 9767 | 100 | 1323 |
| 11 | 5 | 28 | 65500 | 65500 | 18700 | 11 | 18700 | 9 | 9367 | 4 | 9367 | 4 | 9367 | 100 | 1310 |
| 12 | 5 | 33 | 68500 | 68500 | 19300 | 14 | 19300 | 11 | 9967 | 4 | 9967 | 4 | 9967 | 100 | 1305 |
| 13 | 5 | 26 | 64000 | 64000 | 18400 | 9 | 18400 | 9 | 9067 | 4 | 9067 | 4 | 9067 | 100 | 1297 |
| 14 | 5 | 30 | 66500 | 66500 | 18900 | 11 | 18900 | 11 | 9567 | 4 | 9567 | 4 | 9567 | 100 | 1293 |
| 15 | 5 | 28 | 65500 | 65500 | 18700 | 9 | 18700 | 11 | 9367 | 4 | 9367 | 4 | 9367 | 100 | 1291 |
| 16 | 5 | 36 | 70500 | 70500 | 19700 | 14 | 19700 | 14 | 10367 | 4 | 10367 | 4 | 10367 | 100 | 1287 |
| 17 | 5 | 33 | 68500 | 68500 | 19300 | 11 | 19300 | 14 | 9967 | 4 | 9967 | 4 | 9967 | 100 | 1276 |
| 18 | 5 | 31 | 67500 | 67500 | 19100 | 9 | 19100 | 14 | 9767 | 4 | 9767 | 4 | 9767 | 100 | 1276 |

TRACTOR TRAILER 6-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:

| Irc | Axls | Lng | NCS | Weigh | Ax1 | d1 | Ax2 | d2 | Ax 3 | d3 | Ax4 | d4 | Ax5 | d5 | Ax 6 | Span | Mmax |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 6 | 35 | 75000 | 75000 | 18167 | 14 | 15167 | 4 | 15167 | 9 | 8833 | 4 | 8833 | 4 | 8833 | 100 | 1509 |
| 2 | 6 | 37 | 76000 | 76000 | 18333 | 14 | 15333 | 4 | 15333 | 11 | 9000 | 4 | 9000 | 4 | 9000 | 100 | 1502 |
| 3 | 6 | 34 | 74500 | 74500 | 18083 | 11 | 15083 | 4 | 15083 | 11 | 8750 | 4 | 8750 | 4 | 8750 | 100 | 1500 |
| 4 | 6 | 40 | 78000 | 78000 | 18667 | 14 | 15667 | 4 | 15667 | 14 | 9333 | 4 | 9333 | 4 | 9333 | 100 | 1499 |
| 5 | 6 | 32 | 73000 | 73000 | 17833 | 11 | 14833 | 4 | 14833 | 9 | 8500 | 4 | 8500 | 4 | 8500 | 100 | 1496 |
| 6 | 6 | 30 | 72000 | 72000 | 17667 | 9 | 14667 | 4 | 14667 | 9 | 8333 | 4 | 8333 | 4 | 8333 | 100 | 1493 |
| 7 | 6 | 37 | 76000 | 76000 | 18333 | 11 | 15333 | 4 | 15333 | 14 | 9000 | 4 | 9000 | 4 | 9000 | 100 | 1489 |
| 8 | 6 | 32 | 73000 | 73000 | 17833 | 9 | 14833 | 4 | 14833 | 11 | 8500 | 4 | 8500 | 4 | 8500 | 100 | 1488 |
| 9 | 6 | 35 | 75000 | 75000 | 18167 | 9 | 15167 | 4 | 15167 | 14 | 8833 | 4 | 8833 | 4 | 8833 | 100 | 1488 |
| 10 | 6 | 35 | 75000 | 75000 | 18833 | 14 | 18833 | 9 | 9333 | 4 | 9333 | 4 | 9333 | 4 | 9333 | 100 | 1462 |
| 11 | 6 | 32 | 73000 | 73000 | 18500 | 11 | 18500 | 9 | 9000 | 4 | 9000 | 4 | 9000 | 4 | 9000 | 100 | 1449 |
| 12 | 6 | 30 | 72000 | 72000 | 18333 | 9 | 18333 | 9 | 8833 | 4 | 8833 | 4 | 8833 | 4 | 8833 | 100 | 1446 |
| 13 | 6 | 37 | 76000 | 76000 | 19000 | 14 | 19000 | 11 | 9500 | 4 | 9500 | 4 | 9500 | 4 | 9500 | 100 | 1444 |
| 14 | 6 | 34 | 74500 | 74500 | 18750 | 11 | 18750 | 11 | 9250 | 4 | 9250 | 4 | 9250 | 4 | 9250 | 100 | 1442 |
| 15 | 6 | 32 | 73000 | 73000 | 18500 | 9 | 18500 | 11 | 9000 | 4 | 9000 | 4 | 9000 | 4 | 9000 | 100 | 1430 |
| 16 | 6 | 40 | 78000 | 78000 | 19333 | 14 | 19333 | 14 | 9833 | 4 | 9833 | 4 | 9833 | 4 | 9833 | 100 | 1426 |
| 17 | 6 | 37 | 76000 | 76000 | 19000 | 11 | 19000 | 14 | 9500 | 4 | 9500 | 4 | 9500 | 4 | 9500 | 100 | 1416 |
| 18 | 6 | 35 | 75000 | 75000 | 18833 | 9 | 18833 | 14 | 9333 | 4 | 9333 | 4 | 9333 | 4 | 9333 | 100 | 1415 |

TRACTOR TRAILER 7-AXLE GENERATED (POSSIBLE) TRUCK CONFIGURATIONS:

| Trck | Axls | Lngth NCS | Weight Ax1 | d1 | Ax2 | d2 | Ax3 | d3 | Ax4 | d4 | Ax5 | d5 | Ax6 | d6 | Ax7 | Span | Mmax |  |  |
| :---: | :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 1 | 7 | 34 | 80000 | 80000 | 17714 | 9 | 14714 | 4 | 14714 | 9 | 8214 | 4 | 8214 | 4 | 8214 | 4 | 8214 | 100 | 1609 |
| 2 | 7 | 36 | 80000 | 80000 | 17714 | 11 | 14714 | 4 | 14714 | 9 | 8214 | 4 | 8214 | 4 | 8214 | 4 | 8214 | 100 | 1591 |
| 3 | 7 | 36 | 80000 | 80000 | 17714 | 9 | 14714 | 4 | 14714 | 11 | 8214 | 4 | 8214 | 4 | 8214 | 4 | 8214 | 100 | 1576 |
| 4 | 7 | 39 | 80000 | 80000 | 17714 | 14 | 14714 | 4 | 14714 | 9 | 8214 | 4 | 8214 | 4 | 8214 | 4 | 8214 | 100 | 1565 |
| 5 | 7 | 34 | 80000 | 80000 | 17714 | 9 | 8214 | 4 | 8214 | 4 | 8214 | 4 | 8214 | 9 | 14714 | 4 | 14714 | 100 | 1563 |
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| 22 | 7 | 41 | 80000 | 80000 | 17714 | 14 | 8214 | 4 | 8214 | 4 | 8214 | 4 | 8214 | 11 | 14714 | 4 | 14714 | 100 | 1489 |
| 23 | 7 | 43 | 80000 | 80000 | 14000 | 11 | 11000 | 4 | 11000 | 11 | 11000 | 4 | 11000 | 9 | 11000 | 4 | 11000 | 100 | 1488 |


| 24 | 7 | 44 | 80000 | 80000 | 14000 | 9 | 00 | 4 | 00 | 9 | 1000 | 4 | 1000 | 14 | 1000 |  | 000 | 00 | 1483 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 7 | 44 | 80000 | 80000 | 17714 | 14 | 14714 | 4 | 14714 | 14 | 8214 | 4 | 8214 | 4 | 8214 | 4 | 8214 | 100 | 1483 |
| 26 | 7 | 46 | 80000 | 80000 | 14000 | 14 | 11000 | 4 | 11000 | 9 | 11000 | 4 | 11000 | 11 | 11000 | 4 | 1100 | 10 | 1481 |
| 27 | 7 | 43 | 8000 | 80000 | 14000 | 9 | 11000 | 4 | 11000 | 11 | 11000 | 4 | 11000 | 11 | 11000 | 4 | 11000 | 100 | 1480 |
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| 31 | 7 | 46 | 8000 | 8000 | 1400 | 11 | 11000 | 4 | 11000 | 9 | 11000 | 4 | 11000 | 14 | 11000 |  | 11000 | 10 | 1469 |
| 32 | 7 | 46 | 800 | 8000 | 140 | 14 | 1100 | 4 | 1100 | 11 | 1100 | 4 | 000 | 9 | 00 |  | 11000 | 100 | 1467 |
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| 57 | 7 | 48 | 800 | 80 | 162 | 11 | 6952 | 4 | 69 | 4 | 69 | 11 | 13286 |  | 1328 | 14 | 16286 | 100 | 1395 |
| 58 | 7 | 48 | 80000 | 80000 | 1628 | 14 | 6952 | 4 | 6952 | 4 | 6952 | 11 | 13286 | 4 | 1328 | 1 |  | 100 | 139 |
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| 60 | 7 | 51 | 800 | 80000 | 14000 | 14 | 11000 | 4 | 11000 | 14 | 11000 | 4 | 11000 | 11 | 1100 |  | 000 | 100 | 139 |
| 61 | 7 | 44 | 800 | 8000 | 162 | 9 | 6952 | 4 | 6952 | 4 | 6952 | 14 | 13286 |  | 13286 |  | 16286 | 100 | 13 |
| 62 | 7 | 51 | 800 | 80000 | 14000 | 11 | 11000 | 4 | 11000 | 14 | 11000 | 4 | 11000 | 14 | 1100 |  | 11000 | 100 | 1379 |
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| 64 | 7 | 46 | 80 | 80 | 16 | 11 | 69 | 4 | 695 | 4 | 69 | 14 | 13286 |  | 132 |  | 16286 | 100 | 1371 |
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| 66 | 7 | 54 | 80000 | 80000 | 1400 | 14 | 11000 | 4 | 11000 | 14 | 11000 | 4 | 11000 | 14 | 1100 | 4 | 110 | 10 | 135 |
| 67 | 7 | 48 | 800 | 80000 | 162 | 11 | 6952 | 4 | 6952 | 4 | 6952 | 14 | 13286 |  | 13286 | 11 | 16 | 100 | 135 |
| 68 | 7 | 49 | 80000 | 80000 | 16286 | 14 | 6952 | 4 | 6952 | 4 | 6952 | 14 | 13286 |  | 13286 | 9 | 16286 | 100 | 134 |
| 69 | 7 | 49 | 80000 | 80000 | 16286 | 9 | 6952 | 4 | 6952 | 4 | 6952 | 14 | 13286 | 4 | 1328 | 14 | 1628 | 100 | 134 |
| 70 | 7 | 51 | 80000 | 80000 | 16286 | 14 | 6952 | 4 | 6952 | 4 | 6952 | 14 | 13286 | 4 | 13286 | 11 | 16286 | 100 | 133 |
| 71 | 7 | 51 | 80000 | 80000 | 16286 | 11 | 6952 | 4 | 6952 | 4 | 6952 | 14 | 13286 | 4 | 13286 | 14 | 16286 | 100 | 133 |
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